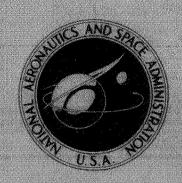
NASA TECHNICAL MEMORANDUM



NASA TM X-3342

OVERALL AND BLADE ELEMENT PERFORMANCE OF A 1.20 PRESSURE RATIO FAN STAGE WITH ROTOR BLADES RESET -7°

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| 1. Report No. NASA TM X-3342 | 2. Government Access | ion No. | 3. Recipient's Catalog | No. |
|---|---------------------------------|----------------------------|------------------------------|------------------|
| 4. Title and Subtitle OVERALL AND BLADE ELEMI | ENT PERFORMA | NCE | 5. Report Date March 1976 | |
| OF A 1, 20 PRESSURE RATIO I | AN STAGE | - | 6. Performing Organiz | ation Code |
| WITH ROTOR BLADES RESET | | | • | |
| 7. Author(s) | | | 8. Performing Organiza | ation Report No. |
| George W. Lewis and George K | lovich | | E-8063 | |
| - | | | 10. Work Unit No. | |
| 9. Performing Organization Name and Address Lewis Research Center | | | 505-04 | |
| National Aeronautics and Space | Administration | | 11. Contract or Grant | No. |
| Cleveland, Ohio 44135 | Manning Cation | | | |
| | | | 13. Type of Report an | d Period Covered |
| 12. Sponsoring Agency Name and Address National Aeronautics and Space | Administration | | Technical Me | morandum |
| Washington, D. C. 20546 | | | 14. Sponsoring Agency | Code |
| | | | | |
| 15. Supplementary Notes | | | | |
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| 16. Abstract | | | | |
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| Hamilton Standard Division of U | | | | |
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| | | | | |
| 17. Key Words (Suggested by Author(s)) | | 18. Distribution Statement | - | |
| Compressors | | Unclassified - v | ınlimited | |
| Turbomachinery | | STAR Category | 02 | |
| Axial flow | | | | |
| Fans | | | | |
| 19. Security Classif, (of this report) | | | | |
| | 20. Security Classif. (d | of this page) | 21. No. of Pages | 22, Price* |

OVERALL AND BLADE ELEMENT PERFORMANCE OF A 1.20 PRESSURE RATIO FAN STAGE WITH ROTOR BLADES RESET -70

by George W. Lewis and George Kovich

Lewis Research Center

SUMMARY

A 51-centimeter-diameter model of a fan stage for short-haul aircraft was tested in a single-stage compressor research facility at Lewis. This stage was designed and built on contract by the Hamilton Standard Division of United Technologies Corporation. In the present study the rotor blades, which were adjustable through axial position, were set 7^0 toward the axial direction (opened) from design setting angle. Surveys of the air flow conditions ahead of the rotor, between the rotor and stator, and behind the stator were made over the stable operating range of the stage. At the design speed of 213.3 meters per second and weight flow of 30.9 kilograms per second, the stage pressure ratio was 1.205 and the efficiency was 0.85. The design speed rotor peak efficiency of 0.90 occurred at a flow rate of 32.5 kilograms per second.

INTRODUCTION

NASA is currently evaluating short-haul aircraft for commercial application. These aircraft must have an efficient and reliable propulsion system satisfying the low-noise requirements for urban communities. The aircraft engines must be capable of a variety of operating conditions: take-off, cruise, approach, and thrust reversal on landing.

In support of this program the Lewis Research Center is investigating a variety of fan compressor inlet stages. These stages provide the potential for high bypass flows in aircraft engines. The Hamilton Standard Division of United Technologies Corporation has designed a fan stage under contract from which two stages were built with adjustable rotor blades: a 197-centimeter-diameter version for acoustic studies (ref. 1) and a 51-centimeter-diameter stage for aerodynamic studies. Overall performance for this

stage at three rotor blade setting angles was reported in reference 2. Results indicated that the overall performance changed with rotor blade setting angle. The overall and blade-element performances at design and design -5° rotor blade setting angles were presented in references 3 and 4, respectively. This report presents the overall and blade-element performance results for the stage with rotor blades set at design -7° . Data are presented over the stable operating range at 3 speeds: 80, 90, and 100 percent of design speed. The data in this report are presented in plotted and in tabular form. The symbols and equations are defined in appendixes A and B. The tests were conducted in the single-stage compressor test facility at Lewis.

APPARATUS AND PROCEDURE

Compressor Test Facility

The compressor stage was tested in the single-stage compressor facility, which is described in detail in reference 5 and shown schematically in figure 1. Atmospheric air enters the test facility at an inlet located on the roof of the building, passes through the flow measuring orifice and into the plenum chamber upstream of the test stage. The air then passes through the experimental compressor stage into the collector and is exhausted to the atmosphere. Weight flow is controlled by a sleeve valve located in the discharge collector.

The adjustable rotor blade test stage was designed and built by Hamilton Standard. A detailed description of the aerodynamic design was presented in reference 3. The design tables are presented herein (tables I to V) for convenience, and the flow path is shown in figure 2. The definitions and units used for the tabular data are presented in appendix C. Briefly, the fan stage was designed for a pressure ratio of 1.20, a rotor tip speed of 213.3 meters per second, and a weight flow per unit annulus area of 195.3 kilograms per second per square meter. For the present test the rotor blades were opened 7°, and this configuration is designated stage 55B-55. The design tables do not reflect the 7° reset.

Instrumentation

The compressor weight flow was determined from measurements on a calibrated thin-plate orifice. The orifice temperature was determined from an average of two Chromel-Constantan thermocouples. Orifice pressures were measured by calibrated transducers.

Radial surveys of the flow were made upstream of the rotor, between the rotor and stator, and downstream of the stator (see fig. 2 for axial location). Total pressure, total temperature, and flow angle were measured with the combination probe (fig. 3(a)), and the static pressure was measured with a 8° C-shaped wedge probe (fig. 3(b)). Each probe was equipped with a null-balancing, control system. The thermocouple material was Chromel-Constantan. Two combination probes and two wedge static probes were used at each of the three measuring stations.

Inner and outer wall static-pressure taps were located at the same axial stations as the survey probes. The circumferential locations of both types of survey probes along with inner and outer wall static-pressure taps are shown in figure 4. An electronic speed counter, in conjunction with a magnetic pickup, was used to measure rotative speed (rpm). The estimated errors of the data, based on inherent accuracies of the instrumentation and recording systems, are as follows:

| Flow, kg/sec |
|---|
| Rotative speed, rpm |
| Flow angle, deg |
| Temperature, K |
| Rotor-inlet total pressure, N/cm ² ±0.01 |
| Rotor-outlet total pressure, N/cm ² |
| Stator-outlet total pressure, N/cm ² |
| Rotor-inlet static pressure, N/cm ² |
| Rotor-outlet static pressure, N/cm ² ±0.07 |
| Stator-outlet static pressure, N/cm ² |

Test Procedure

The stage survey data were taken over a range of weight flow from maximum flow to the near-stall conditions. At 80, 90, and 100 percent of design speed, radial surveys were taken at five weight flows. Data were recorded at nine radial positions for each speed and weight flow.

At each radial position the two combination probes behind the stator were circumferentially traversed to nine different locations across the stator gap. The wedge probes were set at midgap because preliminary studies showed that the static pressure across the stator gap was constant. Values of total pressure, total temperature, and flow angle were recorded at each circumferential position. At the last circumferential position, values of pressure, temperature, and flow angle were also recorded at stations 1 and 2. All probes were then moved to the next radial position, and the circumferential traverse procedure repeated.

Stall was determined at each rotative speed by closing the sleeve valve in the collector until an abrupt drop in total-pressure ratio occurred. Survey data were obtained at a weight flow within 1/2 kilogram of actual stall weight flow.

Calculation Procedure

Measured total temperatures and total pressures were corrected for Mach number and streamline slope. These corrections were based on the instrument probe calibrations given in reference 6. The stream static pressure was corrected for Mach number and streamline slope based on an average calibration for the type of probe used.

Because of the physical construction of the C-shaped static-pressure wedges, it was not possible to obtain static-pressure measurements at 5, 10, and 95 percent of span from the rotor tip. The static pressure at 95 percent span was obtained by assuming a linear variation in static pressure between the values at the inner wall and the probe measurement at 90 percent span. A similar variation was assumed between the static-pressure measurements at the outer wall and the 15-percent span position to obtain the static pressure at 5 and 10 percent spans positions.

At each radial position averaged values of the nine circumferential measurements of total pressure, temperature, and flow angle downstream of the stator (station 3) were obtained. The nine values of total temperature were mass averaged to obtain the stage total-temperature rise. The nine values of total pressure were energy averaged. The measured values of pressure, temperature, and flow angle were used to calculate axial and tangential velocities at each circumferential position. The flow angles presented for each radial position are calculated based on the mass-average of the axial and tangential velocities. To obtain the overall performance, the radial values of total temperature were mass averaged, and the values of total pressure were energy averaged. At each measuring station the integrated weight flow was computed based on the radial survey data. The data, measured at the three measuring stations, have been translated to planes approximating the blade leading and trailing edges by the method presented in reference 7.

Orifice weight flow, total pressures, static pressures, and temperatures were all corrected to sea-level standard-day conditions based on the rotor inlet conditions.

RESULTS AND DISCUSSION

The results from this investigation will be presented in three main sections. The overall performances for the rotor and the stage are given first. Radial distributions

of several performance parameters are then presented for the rotor and stator followed by the blade-element data. The data presented are computer plotted, and occasionally a data point will be omitted because it falls outside the range of the parameters shown in the figure. A brief discussion of the results is included.

All the plotted data, together with some additional performance parameters, are listed in tabular form. The overall performance data are presented in table VI. The blade-element data are given first for the rotor and then for the stator in tables VII and VIII. The abbreviations and units used for the tabular data are defined in appendix C.

Overall Performance

The overall performance for rotor 55B and stage 55B-55 are presented in figures 5 and 6, respectively. Data are presented for 80, 90, and 100 percent of design speed. At each speed line data were taken at five values of weight flow from choke to the near-stall conditions. Design-point values for the original design blade setting angle are shown as solid symbols in both figures for reference purposes and assessment of test results.

Rotor. - The peak efficiency for rotor 55B at design speed was 0.90 and occurred at a weight flow of 32.5 kilograms per second (203 (kg/sec)/m² annulus area). Corresponding values of total-pressure ratio and total-temperature ratio are 1.220 and 1.065, respectively. A peak rotor efficiency of 0.933 occurs at 80 percent of design speed.

<u>Stage</u>. - The peak efficiency for stage 55B-55 at design speed was 0.85 and occurred at a pressure ratio of 1.205 and a weight flow of 30.9 kilograms per second. Peak stage efficiency of 0.91 occurred at 80 percent of design speed.

Radial Distributions

The radial distributions of several parameters are presented at design speed in figure 7 for rotor 55B and in figure 8 for stator 55. In each figure data are presented for three weight flows: near maximum, peak efficiency, and near stall. Temperature-rise efficiency, temperature ratio, pressure ratio, mean incidence angle, meridional velocity ratio, deviation angle, total-loss parameter, total-loss coefficient, and diffusion factor are presented as functions of percent span from the blade tip. The design values for the original stage are shown as solid symbols and are included for reference only. A line is drawn through the data for the peak efficiency weight flow of 30.9 kilograms per second.

Rotor. - At design speed and a weight flow of 30.9 kilograms per second, the energy input was slightly greater than reference values at all span locations, and the pressure ratio is greater except at the 10 and 15 percent spans where reference and measured values are close or equal. At this weight flow the blading is operating at a high incidence angle and the total-pressure loss coefficients are high at all radial stations as compared with the reference values. At the near stall weight flow of 27.8 kilograms per second, high total-pressure loss coefficients and loading is measured from the rotor tip through 30 percent span.

Stator. - At design speed and stage peak efficiency flow (fig. 8) the stator losses are high from the blade tip to the 30 percent span, comparable to reference at 50 and 70 percent spans, and low from 85 percent span to the hub. Incidence angles across the span are higher than the reference values. Blade loading is greater than reference values at the blade tip region and lower in the hub region. With decreasing weight flow greater loading occurs across the blade span and losses decrease from the tip to 15 percent span and increase from 30 percent span to the hub.

Variations With Incidence Angle

The variations of blade-element performance parameters with incidence angle are shown in figure 9 for rotor 55B and in figure 10 for stator 55. The data are presented for 80 and 100 percent of design speed at blade elements located at 5, 10, 30, 50, 70, 90, and 95 percent of blade span as measured from the rotor outlet blade tip. Referenced values are indicated by solid symbols.

Rotor. - The 7° reset shifts the rotor incidence angle to higher positive values than reference for both 80 and 100 percent speeds. Design speed energy addition equalled or exceeded the referenced value over the entire incidence angle range. The total-pressure ratio also equalled or exceeded the reference values at all span locations except at the 5 and 10 percent spans where pressure ratio fell off at the maximum and minimum incidence angle. Minimum total-pressure loss coefficient occurs near or at minimum incidence angle at the 5, 10, and 30 percent spans. The total-pressure loss coefficients are low and indicate little change with incidence angle at the 50 and 70 percent span. At the hub (90 and 95 percent span) total-pressure loss coefficients are high at low incidence angle and decrease with increasing incidence angle.

<u>Stator.</u> - The stator performance with incidence angle is presented in figure 10 for 80 and 100 percent of design speeds. The highest total-pressure loss coefficients occurred at the 5 percent span at maximum flow for both speeds, and this loss coefficient decreased rapidly with increasing incidence angle at the 5, 10, and 30 percent spans.

At 90 and 95 percent spans total-pressure loss coefficients are lower than reference values over the incidence angle range.

SUMMARY OF RESULTS

This report presents the aerodynamic design, the overall performance, and bladeelement performance of 51-centimeter-diameter fan stage suitable for application in short-haul aircraft. Radial surveys of the flow conditions at the rotor inlet, rotor outlet, and stator outlet were made over the stable operating flow range of the stage at equivalent rotative speeds from 80 to 100 percent of design speed. Weight flow and performance parameters were calculated across nine selected blade elements. The following principle results were obtained:

- 1. The stage design speed peak efficiency of 0.85 was obtained at a weight flow of 30.9 kilograms per second and a pressure ratio of 1.20. Peak design speed rotor efficiency of 0.90 occurs at 32.5 kilograms per second and at a pressure ratio of 1.220.
- 2. The energy input across the rotor span exceeds the reference values at design speed and weight flow. The total-pressure loss coefficient at this condition is larger than the reference values across the span.
- 3. Design speed stator total-pressure loss coefficients are high at low incidence angles at the 5, 10, and 30 percent spans and decrease rapidly with increasing incidence angle. Losses in the hub region are generally lower than the reference values.

Lewis Research Center.

National Aeronautics and Space Administration, Cleveland, Ohio, October 2, 1975, 505-04.

APPENDIX A

SYMBOLS

| A _{an} | annulus area at rotor leading edge |
|------------------|--|
| ${f A_f}$ | frontal area at rotor leading edge |
| $C_{\mathbf{p}}$ | specific heat at constant pressure |
| c | aerodynamic chord, cm |
| D | diffusion factor |
| ⁱ mc | mean incidence angle, angle between inlet air direction and line tangent to blade mean camber line at leading edge, deg |
| N | rotative speed, rpm |
| P | total pressure, N/cm ² |
| p | static pressure, N/cm ² |
| \mathbf{r} | radius, cm |
| t | total temperature, K |
| U | wheel speed, m/sec |
| V | air velocity, m/sec |
| W | weight flow, kg/sec |
| ${f z}$ | axial distance references from rotor blade hub leading edge, cm |
| $^{lpha}{ m c}$ | cone angle, deg |
| $^{lpha}{ m s}$ | slope of streamline, deg |
| β | air angle, angle between air velocity and axial direction, deg |
| β 'c | relative meridional air angle based on cone angle, arctan (tan $\beta_m^i \cos \alpha_c/\cos \alpha_s$), deg |
| γ | ratio of specific heats |
| δ | ratio of rotor inlet total pressure to standard pressure of 10.13 $\mathrm{N/m}^2$ |
| δ | deviation angle, angle between exit air direction and tangent to blade mean camber line at trailing edge, deg |
| 0 | ratio of rotor inlet total temperature to standard temperature of 288.2 K |
| η | efficiency |
| | |

 κ_{mc} angle between the blade mean camber line and the meridional plane, deg

σ solidity, ratio of chord to spacing

 $\overline{\omega}$ total loss coefficient

 $\overline{\omega}_{\mathrm{p}}$ profile loss coefficient

 $\overline{\omega}_{_{
m S}}$ shock loss coefficient

Subscripts:

ad adiabatic (temperature rise)

id ideal

LE blade leading edge

m meridional direction

mom momentum rise

p polytropic

TE blade trailing edge

z axial direction

 θ tangential direction

1 instrumentation plane upstream of rotor

2 instrumentation plane between rotor and stator

3 instrumentation plane downstream of stator

Superscript:

' relative to blade

APPENDIX B

EQUATIONS

Performance parameters are defined as follows:

Mean incidence angle

$$i_{mc} = (\beta'_c)_{LE} - (\kappa_{mc})_{LE}$$
(B1)

Deviation angle

$$\delta^{O} = (\beta_{C}^{\dagger})_{TE} - (\kappa_{mc})_{TE}$$
 (B2)

Diffusion factor

$$D = 1 - \frac{V_{TE}'}{V_{LE}'} + \left| \frac{(rV_{\theta})_{TE} - (rV_{\theta})_{LE}}{(r_{TE} + r_{LE})\sigma(V_{LE}')} \right|$$
(B3)

Total loss coefficient

$$\frac{\dot{\omega}}{\omega} = \frac{(P_{id}^{!})_{TE} - (P^{!})_{TE}}{P_{LE}^{!} - p_{LE}}$$
(B4)

Profile loss coefficient

$$\overline{\omega}_{\mathbf{p}} = \overline{\omega} - \overline{\omega}_{\mathbf{S}}$$
 (B5)

Total loss parameter

$$\frac{\overline{\omega}\cos(\beta'_{\rm m})_{\rm TE}}{2\sigma} \tag{B6}$$

Profile loss parameter

$$\frac{\overline{\omega}_{p} \cos (\beta'_{m})_{TE}}{2\sigma}$$
 (B7)

Adiabatic (temperature-rise) efficiency

$$\eta_{\text{ad}} = \frac{\left(\frac{P_{\text{TE}}}{P_{\text{LE}}}\right)^{(\gamma-1)/\gamma} - 1}{\frac{T_{\text{TE}}}{T_{\text{LE}}} - 1}$$
(B8)

Momentum-rise efficiency

$$\eta_{\text{mom}} = \frac{\left(\frac{P_{\text{TE}}}{P_{\text{LE}}}\right)^{(\gamma-1)/\gamma} - 1}{\frac{(UV_{\theta})_{\text{TE}} - (UV_{\theta})_{\text{LE}}}{T_{\text{LE}}C_{\text{p}}}}$$
(B9)

Equivalent weight flow

$$\frac{W\sqrt{\theta}}{\delta}$$
 (B10)

Equivalent rotative speed

$$\frac{N}{\sqrt{\theta}}$$
 (B11)

Weight flow per unit annulus area

$$\underbrace{\begin{pmatrix} \mathbf{W} \mathbf{\sqrt{\theta}} \\ \mathbf{\delta} \end{pmatrix}}_{\mathbf{A}_{an}} \tag{B12}$$

Weight flow per unit frontal area

$$\underbrace{\begin{pmatrix} \mathbf{W} \mathbf{V}_{\theta} \\ \delta \end{pmatrix}}_{\mathbf{A}_{\mathbf{f}}} \tag{B13}$$

Head-rise coefficient

$$\frac{C_{p}T_{LE}}{U_{tip}^{2}}\left[\left(\frac{P_{TE}}{P_{LE}}\right)^{(\gamma-1)/\gamma} - 1\right]$$
 (B14)

Flow coefficient

$$\left(\frac{V_{z}}{U_{tip}}\right)_{LE}$$
 (B15)

Polytropic efficiency

$$\eta_{\mathbf{p}} = \frac{\ln\left(\frac{\mathbf{P}_{\mathrm{TE}}}{\mathbf{P}_{\mathrm{LE}}}\right)^{(\gamma-1)/\gamma}}{\ln\left(\frac{\mathbf{T}_{\mathrm{TE}}}{\mathbf{T}_{\mathrm{LE}}}\right)}$$
(B16)

APPENDIX C

DEFINITIONS AND UNITS USED IN TABLES

ABS absolute

AERO CHORD straight line between blade leading and trailing edges along

design streamline, cm

AREA RATIO ratio of actual flow area to critical area (where local Mach

number is one)

BETAM meridional air angle, deg

CONE ANGLE angle between axial direction and conical surface representing

blade element, deg

DEV deviation angle (defined by eq. (B2)), deg

D-FACT diffusion factor (defined by eq. (B3)

EFF adiabatic efficiency (defined by eq. (B8))

IN inlet (leading edge of blade)

INCIDENCE incidence angle (mean defined by eq. (B1)), deg

KIC angle between blade mean camber line at leading edge and

meridional plane, deg

KOC angle between blade mean camber line at trailing edge and

meridional plane, deg

KTC angle between blade mean camber line at transition point and

meridional plane, deg

LOSS COEFF loss coefficient (total defined by eq. (B4) and profile defined

by eq. (B5))

LOSS PARAM loss parameter (total defined by eq. (B6) and profile defined

by eq. (B7))

MERID meridional

MERID VEL R meridional velocity ratio

OUT outlet (trailing edge of blade)

PERCENT SPAN percent of blade span from tip at rotor outlet

PHISS suction surface camber ahead of assumed shock locagion, deg

PRESS pressure, N/cm²

PROF profile

RADII radius, cm

REL relative to the blade

RI inlet radius (leading edge of blade), cm

RO outlet radius (trailing edge of blade), cm

RP radial position

RPM equivalent rotative speed, rpm

SETTING ANGLE angle between aerodynamic chord and meridional plane, deg

SOLIDITY ratio of aerodynamic chord to blade spacing

SPEED speed, m/sec

SS suction surface

STREAMLINE SLOPE slope of streamline, deg

TANG tangential

TEMP temperature, K

TI thickness of blade at leading edge, cm

TM thickness of blade at maximum thickness, cm

TO thickness of blade at trailing edge, cm

TOT total

TOTAL CAMBER difference between inlet and outlet blade mean camber lines.

deg

VEL velocity, m/sec

WT FLOW equivalent weight flow, kg/sec

X FACTOR ratio of suction surface camber ahead of assumed shock loca-

tion of multiple circular arc blade section to that of double

circular arc blade section

ZIC axial distance to blade leading edge from inlet, cm

ZMC axial distance to blade maximum thickness point from inlet, cm

ZOC axial distance to blade trailing edge from inlet, cm

ZTC axial distance to transition point from inlet, cm

REFERENCES

- 1. Woodward, Richard P.; Glaser, Frederick W.; and Wasniak, Joseph A.: Noise Comparisons of Two 1.2-Pressure-Ratio Fans with 15 and 42 Rotor Blades. NASA TM X-2891, 1973.
- 2. Lewis, George W.; Moore, Royce D.; and Kovich, George: Performance of a 1.2-Pressure-Ratio STOL Fan Stage at Three Rotor Blade Setting Angles. NASA TM X-2837, 1973.
- 3. Lewis, George W., Jr.; and Tysl, Edward R.: Overall and Blade-Element Performance of a 1.20-Pressure-Ratio Fan Stage with Rotor Blades at Design Setting Angle. NASA TM X-3101, 1974.
- 4. Lewis, George W., Jr.; Osborn, Walter M.; and Moore, Royce D.: Overall and Blade-Element Performance of a 1.20-Pressure-Ratio Fan Stage with Rotor Blades Reset -5°. NASA TM X-3338, 1975. (E-8057)
- 5. Urasek, Donald C.; and Janetzke, David C.: Performance of Tandem-Bladed Transonic Compressor Rotor with Tip Speed of 1375 Feet per Second. NASA TM X-2484, 1972.
- 6. Glawe, George E.; Krause, Lloyd M.; and Dudzinski, Thomas J.: A Small Combination Sensing Probe for Measurement of Temperature, Pressure, and Flow Direction. NASA TN D-4816, 1968.
- 7. Ball, Calvin L.; Janetske, David C.; and Reid, Lonnie: Performance of 1380 Foot-Per-Second Tip-Speed Axial-Flow Compressor Rotor Blade with Tip Solidity of 1.5. NASA TM X-2379, 1972.

TABLE I. - DESIGN OVERALL PARAMETERS

FOR STAGE 55-55

| ROTOR TOTAL PRESSURE RATIO | 1.205 |
|---------------------------------|--------|
| STAGE TOTAL PRESSURE RATIO | 1.196 |
| | |
| ROTOR TOTAL TEMPERATURE RATIO | 1.058 |
| STAGE TOTAL TEMPERATURE RATIO | 1.058 |
| ROTOR ADIABATIC EFFICIENCY | 0.940 |
| STAGE ADIABATIC EFFICIENCY | 0.903 |
| ROTOR POLYTROPIC EFFICIENCY | 0.941 |
| STAGE POLYTROPIC EFFICIENCY | 0.906 |
| ROTOR HEAD RISE COEFFICIENT | 0.348 |
| STAGE HEAD RISE COEFFICIENT | 0.334 |
| FLOW COEFFICIENT | 0.861 |
| WT FLOW PER UNIT FRONTAL AREA 1 | 53.970 |
| WT FLOW PER UNIT ANNULUS AREA | 95.295 |
| WT FLOW | 31.207 |
| RPM 80 | 20.000 |
| | 13.323 |

TABLE II. – DESIGN BLADE-ELEMENT PARAMETERS FOR ROTOR 55

| RP TIP 1 2 3 4 5 6 7 8 9 HVB | RAD IN 25.400 24.730 24.026 23.323 21.172 18.320 15.539 13.541 12.907 12.288 11.684 | OUT 25.400 24.714 24.028 23.343 21.285 18.542 15.799 13.741 13.056 12.370 | ABS IN 0. 0. -0. -0. -0. -0. -0. -0. | BETAM 0UT 27.6 28.8 29.7 30.4 31.6 32.9 34.7 36.1 36.6 37.1 37.6 | IN 48.4 47.8 | BETAM OUT 38.1 34.9 32.1 29.7 24.1 16.6 7.9 1.4 -0.7 -2.8 -4.8 | IN 288.2 288.2 288.2 288.2 288.2 288.2 288.2 288.2 | RATIO 1.063 1.065 1.067 1.067 1.064 1.057 1.051 1.044 1.042 | TOTAL IN 10.14 10.14 10.14 10.14 10.14 10.14 10.14 10.14 | PRESS RATIO 1.213 1.226 1.235 1.238 1.231 1.208 1.178 1.144 1.130 1.115 1.098 |
|---|---|---|--|--|---|---|--|---|---|---|
| RP TIP 1 2 3 4 5 6 7 8 9 HUB | IN 189.4 188.1 186.9 185.9 183.6 181.8 181.3 182.0 182.6 183.2 | VEL 0UT 184.1 190.0 194.1 196.3 197.6 196.3 194.5 189.8 187.2 184.1 180.4 | IN 285.3 280.2 275.0 270.1 255.6 238.2 223.4 214.7 212.3 | VEL 0UT 207.3 203.0 198.9 194.9 184.4 172.0 161.4 153.5 150.4 147.0 143.4 | MER II IN 189.4 188.1 186.9 185.9 183.6 181.8 181.3 182.0 182.6 183.2 183.9 | VEL OUT 163.1 166.5 168.6 169.3 164.8 159.9 153.5 150.4 146.9 | TAN IN 0000000. 0. | 91.5 96.2 99.4 103.6 110.6 111.7 111.5 111.0 | WHEEL IN 213.3 207.7 201.8 195.9 177.8 153.9 130.5 113.7 108.4 103.2 98.1 | SPEED OUT 213.3 207.6 201.8 196.0 178.8 155.7 132.7 115.4 109.6 103.9 98.1 |
| RP TIP 1 2 3 4 5 6 7 8 9 | ABS M IN 0.575 0.570 0.567 0.563 0.556 0.550 0.551 0.553 0.555 | ACH NO OUT 0.540 0.557 0.570 0.577 0.582 0.576 0.563 0.555 0.546 | REL M 1N 0.865 0.850 0.834 0.818 0.774 0.721 0.676 0.650 0.643 0.637 0.631 | 0.595 0.584 0.573 0.543 0.508 0.478 0.445 0.446 0.436 | MERID M. 1N 0.575 0.570 0.567 0.563 0.556 0.550 0.549 0.551 0.553 0.555 | ACH NO OUT 0.478 0.488 0.495 0.497 0.496 0.487 0.473 0.455 0.446 0.424 | STREAML I IN 0.78 0.66 0.61 0.62 0.85 1.26 1.39 1.04 0.78 0.44 0.05 | NE SLOPE OUT 0.46 0.55 0.66 0.79 1.14 1.43 1.40 0.98 0.71 0.37 -0.03 | MERID VEL R 0.861 0.885 0.902 0.911 0.917 0.907 0.882 0.843 0.824 0.802 0.777 | |
| RP TIP 1 2 3 4 5 6 7 8 9 HUB | PERCENT SPAN 0. 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INC I MEAN -2.0 -2.4 -2.9 -3.2 -3.6 -3.7 -3.9 -2.4 -1.7 -0.9 | DENCE | DEV 6.1 7.2 8.0 8.5 10.5 12.6 12.4 12.3 12.0 | D-FACT 0.441 0.458 0.470 0.479 0.493 0.503 0.512 0.517 0.520 0.524 0.529 | EFF 0.903 0.917 0.928 0.936 0.958 0.970 0.949 0.884 0.792 0.724 | LOSS C TOT 0.051 0.047 0.043 0.039 0.027 0.019 0.032 0.070 0.090 0.116 0.145 | 0EFF PROF 0.051 0.047 0.043 0.039 0.027 0.019 0.032 0.070 0.090 0.116 0.145 | LOSS P TOT 0.023 0.022 0.020 0.019 0.013 0.009 0.015 0.031 0.039 0.049 0.059 | ARAM PROF 0.023 0.022 0.020 0.019 0.015 0.031 0.039 0.049 0.059 |

| RP TIP 1 2 3 4 5 6 7 8 9 HUB | RAD IN 25.938 25.231 24.547 23.877 21.847 19.166 16.502 14.518 13.859 13.202 12.548 | 0UT 25.938 25.299 24.672 24.048 22.222 19.826 17.464 15.682 15.069 | ABS IN 27.9 28.9 29.7 30.3 31.2 32.3 34.0 35.4 35.9 36.4 36.9 | BETAM OUT -0. -0. -0. -0. -0. -0. -0. | REL. IN 27.9 28.9 29.7 30.3 31.2 32.3 34.0 35.4 35.9 36.4 36.9 | BETAM OUT -0. 0. -0. -0. -0. -0. -0. -0. | TOTA IN 306.2 307.0 307.5 307.5 306.6 304.7 302.7 301.0 300.3 299.6 298.9 | TEMP RATIO 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 | TOTAL IN 12.29 12.43 12.51 12.55 12.48 12.24 11.94 11.60 11.45 11.30 | PRESS RATIO 0.992 0.992 0.993 0.994 0.997 0.996 0.991 0.985 0.982 0.979 0.976 |
|---|---|--|--|--|--|--|--|---|--|---|
| RP TIP 1 2 3 4 5 6 7 8 9 HUB | ABS IN 178.6 185.4 190.0 192.7 194.8 193.0 189.3 182.6 179.3 175.3 | VEL 0UT 169.2 175.1 178.9 180.8 179.9 172.7 160.6 143.7 135.4 125.7 114.6 | REL IN 178.6 185.4 190.0 192.7 194.8 193.0 189.3 182.6 179.3 175.3 170.9 | VEL 0UT 169.2 175.1 178.9 180.8 179.9 172.7 160.6 143.7 135.4 125.7 114.6 | MERI IN 157.9 162.3 165.1 166.5 166.7 163.1 156.9 148.9 145.3 141.2 | VEL OUT 169.2 175.1 178.9 180.8 179.9 172.7 160.6 143.7 135.4 125.7 | IN 83.5 89.6 94.1 97.2 100.9 103.1 105.9 105.8 | G VEL OUT -0. -0. -0. -0. -0. -0. -0. | WHEEL IN 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. | SPEED OUT O. O. O. O. O. |
| RP TIP 1 2 3 4 5 6 7 8 9 HUB | ABS M IN 0.523 0.543 0.557 0.566 0.573 0.569 0.559 0.540 0.530 0.519 | ACH NO OUT 0.494 0.511 0.523 0.528 0.526 0.506 0.471 0.420 0.396 0.367 0.334 | REL M IN 0.523 0.543 0.557 0.566 0.573 0.569 0.559 0.540 0.530 0.519 0.505 | ACH NO OUT 0.494 0.511 0.523 0.528 0.526 0.506 0.471 0.420 0.396 0.367 0.334 | MERID M IN 0.462 0.475 0.484 0.488 0.490 0.481 0.464 0.440 0.430 0.418 0.404 | ACH NO OUT 0.494 0.511 0.523 0.528 0.526 0.506 0.471 0.420 0.396 0.367 0.334 | STREAMLI IN 0.63 0.86 1.10 1.34 2.08 3.13 4.25 5.10 5.35 5.58 5.80 | NE SLOPE OUT -0.10 0.05 0.22 0.39 0.95 1.72 2.42 2.77 2.76 2.68 2.54 | MERID VEL R 1.071 1.079 1.084 1.086 1.079 1.058 1.024 0.965 0.932 0.839 | |
| RP TIP 1 2 3 4 5 6 7 8 9 HUB | PERCENT SPAN 0. 5.00 10.00 15.00 30.00 70.00 85.00 90.00 95.00 | INCI MEAN -12.5 -11.6 -10.9 -10.3 -9.8 -9.1 -7.8 -6.8 -6.4 -6.0 -5.6 | DENCE | DEV 16.0 15.6 15.3 15.0 14.0 13.0 11.7 10.9 10.7 | D-FACT 0.380 0.385 0.386 0.387 0.382 0.400 0.440 0.464 0.494 | | LOSS C TOT 0.049 0.042 0.036 0.030 0.017 0.018 0.046 0.086 0.103 0.123 0.147 | 0EFF PR0F 0.049 0.042 0.036 0.030 0.017 0.018 0.046 0.086 0.103 0.123 0.147 | LOSS P TOT 0.034 0.029 0.024 0.019 0.010 0.010 0.021 0.035 0.040 0.046 0.052 | ARAM PROF 0.034 0.029 0.024 0.010 0.010 0.021 0.035 0.040 0.046 0.052 |

TABLE IV. - BLADE GEOMETRY FOR ROTOR 55

| RP TIP 1 2 3 4 5 6 7 8 9 | 5. 10. 15. 30. 50. 70. 85. 90. | RI 25.400 24.730 24.026 23.323 21.172 18.320 15.539 13.541 12.907 12.288 | R0 25.400 24.714 24.028 23.343 21.285 18.542 15.799 13.741 13.056 12.370 | KIC 50.40 50.29 50.05 49.67 47.72 43.95 39.62 34.40 32.39 30.27 | 9.69 7.66 | KOC 32.00 27.64 24.05 21.21 13.56 4.41 -4.79 -11.02 -13.01 -14.95 | -0. -0. -0. -0. -0. -0. -0. | CONE ANGLE 0.057 -0.124 0.057 0.152 0.892 1.806 2.239 1.813 1.375 0.769 |
|---|--|--|--|---|---|---|---|--|
| HUB | 100. | 11.684 | 11.684 | 28.06 | 5.61 | -16.84 | 0 | 0.057 |
| RP TIP 1 2 3 4 5 6 7 8 9 HUB | BLADE T1 0.019 0.025 0.031 0.050 0.063 0.083 0.091 0.090 0.088 | TM 0.239 0.264 0.293 0.326 0.441 0.591 0.741 0.839 0.862 0.881 | TO 0.019 0.025 0.031 0.036 0.050 0.063 0.083 0.091 | ZI -0.636 -0.671 -0.685 -0.659 -0.572 -0.371 -0.206 -0.142 -0.073 | ZMC 2.690 2.650 2.658 2.658 2.669 2.753 2.824 | 2.669 2.753 2.824 2.852 | Z0 6.522 6.546 6.588 6.644 6.597 6.455 6.284 6.116 6.057 | |
| RP TIP 1 2 3 4 5 6 7 8 9 HUB | AERO CHORD 9.499 9.274 9.105 8.980 8.428 7.703 6.978 6.458 6.290 6.126 5.966 | 41,14 38,96 37,05 35,44 30,66 24,22 17,48 11,74 9,73 7,69 | 22.65 26.00 28.47 34.15 | SOLIDITY 0.893 0.896 0.905 0.919 0.948 0.998 1.063 1.130 1.157 1.186 1.219 | X FACTOR 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 | ₹. | | |

TABLE V. - BLADE GEOMETRY FOR STATOR 55

| | PERCENT | r RAD | 11(| BL/ | ADE ANGL | ES . | DELTA | CONE |
|-------------|----------------|------------------|----------|----------|----------|----------|--------|---------|
| RP | SPAN | RI | R0 | KIC | KTC | K0C | INC | ANGLE |
| TIP | 0. | 25.938 | 25.938 | 40.40 | 17.86 | -16.01 | -0. | 0.057 |
| 1 | 5. | 25.231 | 25.299 | 40.47 | 18.05 | -15.65 | 0. | 0.378 |
| 2 | 10. | 24.547 | 24.672 | 40.54 | 18.23 | -15.31 | -0. | . 0.693 |
| 3 | 15. | 23.877 | 24.048 | 40.61 | 18.40 | -14.98 | -0. | 0.952 |
| 4 | 30. | 21.847 | 22.222 | 41.00 | 19.02 | -14.04 | -0. | 2.087 |
| 5 | 50. | 19.166 | 19.826 | 41.42 | 19.69 | -13.02 | -0. | 3.692 |
| 6 | 70. | 16.502 | 17.464 | 41.78 | | -11.73 | -0. | 5.406 |
| 7 | | 14.518 | | 42.13 | | -10.93 | -0. | 6.564 |
| 8 | 90. | 13.859 | 15.069 | 42.23 | | -10.66 | -0. | 6.832 |
| 9 | 95. | 13.859 13.202 | 14.447 | 42.32 | | -10.38 | | 7.039 |
| HUB | 100. | 12.548 | 13.818 | 42.40 | 21.48 | -10.10 | 0. | 7.185 |
| | | | | | | | | |
| | | | | | | _ | _ | |
| | BLADE | | | | | IMENSION | | |
| RP | TI | TM | TO | ZI | ZMC | ZTC | Z0 | |
| TIP | 0.188 | 0.953 | 0.087 | | | 25.502 | | |
| 1 | 0.188 | 0.953 | 0.087 | | | 25.489 | | |
| 2 | 0.188 | 0.953 | 0.087 | | | 25.486 | | |
| 3 | 0.188 | 0.953 | 0.087 | | | 25.490 | | |
| & = | 0.188 | 0.953 | 0.087 | | | 25.473 | | |
| 4 5 6 | 0.188 | 0.953 | 0.087 | 21.662 | | | | |
| 7 | 0.188 | 0.953 | 0.087 | | | 25.426 | | |
| | 0.188 | | 0.087 | | | 25.404 | | |
| 8 9 | 0,188 | | 0.087 | | | | | |
| HUB | 0.188 0.188 | 0.953 0.953 | 0.087 | | | | | |
| פטמ | V. 100 | V.900 | V. VO / | ₹1.00A | 23,367 | 25.387 | 31,764 | |
| | | | | | | | | |
| | 1EDA | SETTING | ነ አቸለዋ ና | | X | | | |
| 20 | AERO CHORD | | | SOLIDITY | | > | | |
| RP | 10.584 | | 56.40 | 0.714 | | ` | | |
| ŢĮP | 10.584 | 12.15 | 56.12 | 0.733 | 1.000 | | | |
| 1 2 | 10.584 | 12.36 | 55.85 | 0.753 | 1.000 | | | |
| 3 | 10.584 | 12.57 | 55.59 | 0.773 | 1.000 | | | |
| 4 | 10.584 | 13.28 | 55.04 | 0.841 | 1.000 | | | |
| 5 | 10.585 | 14.07 | 54.44 | 0.951 | 1.000 | | | |
| 6 | 10.586 | 15.00 | 53.51 | 1.091 | 1.000 | | | |
| 7 | 10.588 | 15.67 | 53.06 | 1.228 | 1.000 | | | |
| 8 | 10.588 | 15.88 | 52.88 | 1.282 | 1.000 | | | |
| 9 | 10.589 | 16.09 | 52.69 | 1.341 | 1.000 | | | |
| HUB | 10.589 | 16.30 | 52.50 | 1.406 | 1.000 | | | |
| | | | | ., | ., | | | |

TABLE VI. - OVERALL PERFORMANCE FOR STAGE 55B-55

(a) 80 Percent of design speed

| Parameter | | Reading | | | | | |
|--|--|---|---|---|---|--|--|
| | 1638 | 1639 | 1640 | 1641 | 1642 | | |
| ROTOR TOTAL PRESSURE RATIO STAGE TOTAL PRESSURE RATIO ROTOR TOTAL TEMPERATURE RATIO STAGE TOTAL TEMPERATURE RATIO STAGE TOTAL TEMPERATURE RATIO ROTOR TEMP. RISE EFFICIENCY ROTOR MOMENTUM RISE EFFICIENCY ROTOR HEAD RISE COEFFICIENT STAGE HEAD RISE COEFFICIENT HIT FLOW PER UNIT FRONTAL AREA HIT FLOW PER UNIT ANNULUS AREA HIT FLOW AT ROTOR INLET HIT FLOW AT ROTOR OUTLET HIT FLOW AT STATOR OUTLET HIT FLOW AT STATOR OUTLET ROTATIVE SPEED PERCENT OF DESIGN SPEED | 1.132 1.106 1.039 1.039 0.923 0.748 0.875 0.359 1.201 161.89 205.34 32.81 33.36 33.98 34.69 641.0 | 1.132 1.118 1.039 1.037 0.933 0.893 0.360 0.325 1.037 146.87 186.29 29.77 30.23 30.64 31.46 6396.1 | 1.135 1.125 1.040 1.038 0.924 0.880 0.366 0.341 0.888 130.90 166.04 26.53 26.94 27.29 28.35 6411.9 | 1.137 1.128 1.042 1.039 0.895 0.895 0.858 0.377 0.798 119.46 151.52 24.21 24.70 25.13 26.34 6418.5 | 1.133 1.125 1.043 1.041 0.826 0.786 0.360 0.334 0.697 106.16 134.66 21.52 22.00 22.45 24.27 6417.7 80.0 | | |

(b) 90 Percent of design speed

| Parameter | | - | Reading | | | | | | |
|---|--|---|--|---|---|--|--|--|--|
| | 1636 | 1637 | 1632 | 1633 | 1634 | | | | |
| ROTOR TOTAL PRESSURE RATIO STAGE TOTAL PRESSURE RATIO ROTOR TOTAL TEMPERATURE RATIO STAGE TOTAL TEMPERATURE RATIO ROTOR TEMP. RISE EFFICIENCY ROTOR MOMENTUM RISE EFFICIENCY ROTOR MOMENTUM RISE EFFICIENT STAGE HEAD RISE COEFFICIENT STAGE HEAD RISE COEFFICIENT HEDW COEFFICIENT WIF FLOW PER UNIT FRONTAL AREA WIT FLOW PER UNIT ANNULUS AREA WIT FLOW AT ROTOR INLET WIT FLOW AT ROTOR OUTLET HIT FLOW AT STATOR OUTLET ROTATIVE SPEED PERCENT OF DESIGN SPEED | 1.149 1.129 1.050 1.046 0.806 0.769 0.761 0.318 0.277 1.144 162.90 206.65 33.02 34.68 34.17 35.34 7224.5 | 1.169 1.153 1.050 1.046 0.917 0.897 0.362 0.331 1.000 155.09 196.73 31.44 31.91 32.40 33.50 7175.3 | 1.176 1.161 1.052 1.050 0.903 0.866 0.879 0.371 0.342 0.899 144.59 183.29 29.29 29.78 30.35 31.47 7224.9 | 1.175 1.163 1.053 1.051 0.887 0.866 0.370 0.346 0.820 133.96 169.92 27.15 27.74 28.24 29.63 7208.2 | 1.173 1.160 1.055 1.053 0.850 0.813 0.812 0.365 0.341 123.69 156.90 25.07 25.61 26.20 27.89 7221.5 90.0 | | | | |

(c) 100 Percent of design speed

| Parameter | | | Reading | | | | | |
|--|--|--|---|--|--|--|--|--|
| | 1625 | 1626 | 1627 | 1628 | 1629 | | | |
| ROTOR TOTAL PRESSURE RATIO STAGE TOTAL PRESSURE RATIO ROTOR TOTAL TEMPERATURE RATIO STAGE TOTAL TEMPERATURE RATIO ROTOR TEMP. RISE EFFICIENCY STAGE TEMP. RISE EFFICIENCY ROTOR MOMENTUM RISE EFFICIENCY ROTOR HEAD RISE COEFFICIENT STAGE HEAD RISE COEFFICIENT FLOW COEFFICIENT HT FLOW PER UNIT FRONTAL AREA HT FLOW PER UNIT ANNULUS AREA HT FLOW AT ROTOR INLET HT FLOW AT ROTOR OUTLET HT FLOW AT STATOR OUTLET ROTATIVE SPEED PERCENT OF DESIGN SPEED | 1.209 1.188 1.064 1.063 0.872 0.803 0.837 0.352 0.320 1.010 166.81 211.58 33.81 34.42 35.09 36.41 8039.1 | 1.220 1.201 1.065 1.063 0.905 0.864 0.368 0.358 0.915 203.13 32.46 33.66 35.10 8060.5 | 1.221 1.205 1.066 1.064 0.890 0.852 0.855 0.369 0.343 0.865 152.18 193.03 30.85 31.92 33.56 8072.1 | 1.219 1.203 1.066 1.064 0.872 0.835 0.366 0.341 0.808 145.04 183.97. 29.40 29.85 50.36 32.17 8069.0 | 1.213 1.196 1.068 1.065 0.805 0.783 0.355 0.328 0.747 136.98 173.75 27.76 28.19 28.69 30.79 8080.2 100.8 | | | |

TABLE VII. - BLADE-ELEMENT DATA AT BLADE EDGES FOR ROTOR 55B

(a) 80 Percent of design speed; reading 1638

| RP 1 2 3 4 5 6 7 8 9 | RAD IN 24.729 2 24.026 2 23.322 2 21.173 2 18.321 1 15.540 1 12.906 1 12.289 1 | 0UT 24.714 24.028 23.343 21.285 18.542 15.799 13.741 | ABS IN 0.0 0.0 0.0 0.0 0.0 0.0 | BETAM OUT 20.5 19.7 20.6 23.6 27.2 29.1 30.6 32.3 33.2 | REL IN 39.2 37.6 37.3 34.5 30.9 26.9 23.8 22.9 22.5 | BETAM 0UT 25.8 24.0 22.0 15.1 6.3 -1.2 -6.5 -8.2 -9.4 | IN 289.1 289.0 288.6 288.0 287.8 | RATIO 1.039 1.040 1.041 1.042 1.041 1.037 1.033 1.030 1.028 | IN 9.90 10.13 10.15 10.15 | |
|----------------------|---|--|--|--|--|--|---|--|---|---|
| RP 1 2 3 4 5 6 7 8 9 | ABS IN 203.9 209.2 204.8 206.5 205.7 205.9 206.6 203.8 198.9 | VEL 0UT 206.6 213.4 214.5 220.1 224.7 227.4 223.9 211.8 203.2 | 1N 263.0 264.2 257.6 250.6 239.8 231.0 225.7 | VEL 0UT 214.9 220.1 216.6 208.8 201.0 198.7 193.8 180.9 172.4 | IN 203.9 209.2 204.8 206.5 205.7 | D VEL OUT 193.4 201.0 200.9 201.6 199.8 198.7 192.6 179.0 170.1 | TAN IN 0.1 0.0 0.0 0.0 0.0 0.0 | G VEL OUT 72.5 71.8 75.3 88.2 102.8 110.6 114.1 113.2 | WHEEL IN 166.2 161.4 156.2 142.0 123.3 104.6 90.9 86.3 82.6 | SPEED 0UT 166.1 161.4 156.4 142.7 124.8 106.3 92.3 87.3 83.1 |
| RP 1 23 4 5 6 7 8 9 | ABS MA IN 0.621 0.639 0.624 0.631 0.628 0.629 0.631 0.622 0.606 | OUT 0.617 0.639 0.642 0.661 0.677 0.687 0.638 0.611 | REL M IN 0.801 0.806 0.785 0.765 0.732 0.706 0.690 0.676 0.656 | OUT 0.642 0.659 0.649 0.627 0.605 0.600 0.586 0.545 | MERID M IN 0.621 0.639 0.624 0.631 0.628 0.629 0.631 0.622 0.606 | ACH NO OUT 0.577 0.601 0.601 0.605 0.602 0.600 0.582 0.539 0.512 | | | | PEAK SS MACH NC 0.801 0.806 0.785 0.765 0.732 0.706 0.690 0.676 0.656 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INCI MEAN -4.1 -5.4 -5.3 -6.2 -6.0 -5.7 -3.7 -2.4 -0.7 | DENCE | DEV 5.2 7.0 7.8 8.6 9.1 10.6 11.6 11.8 12.6 | D-FACT 0.337 0.317 0.318 0.353 0.378 0.367 0.366 0.405 0.418 | EFF 1.045 0.964 0.954 0.933 0.926 0.921 0.841 0.636 0.504 | LOSS C TOT -0.017 0.014 0.019 0.029 0.034 0.035 0.065 0.138 0.187 | PR0F | LOSS F TOT -0.009 0.007 0.009 0.015 0.017 0.029 0.059 0.078 | PROF -0.009 0.007 0.009 0.015 0.017 |

(b) 80 Percent of design speed; reading 1639

| RP 1 2 3 4 5 6 7 8 9 | RADII IN OUT 24.729 24.714 24.026 24.028 23.322 23.343 21.173 21.285 18.321 18.542 15.540 15.799 13.541 13.741 12.906 13.056 12.289 12.370 | ABS IN -0.0 0.0 -0.0 -0.0 -0.0 -0.0 -0.0 | BETAM 0UT 23.7 23.2 23.6 26.5 29.8 31.8 34.2 36.0 36.9 | REL IN 43.3 41.7 41.4 38.6 34.7 30.5 27.1 26.1 25.6 | BETAM 0UT 28.8 26.2 24.5 17.9 9.0 0.3 -7.2 -9.0 -11.1 | TOTAL TEMP IN RATIO 289.0 1.042 288.9 1.041 288.6 1.042 287.9 1.041 287.9 1.038 287.9 1.035 287.9 1.034 287.8 1.030 | TOTAL PRESS IN RATIO 9.96 1.149 10.13 1.146 10.15 1.147 10.15 1.142 10.15 1.130 10.15 1.124 10.15 1.112 10.14 1.081 10.09 1.080 |
|----------------------|---|--|---|---|---|---|---|
| RP 1 23 4 5 6 7 8 9 | ABS VEL IN OUT 175.7 182.6 180.0 189.8 177.1 191.4 177.9 193.8 176.7 194.9 176.8 199.2 178.1 201.4 176.4 189.9 172.2 187.5 | REL IN 241.3 241.3 236.2 227.5 215.0 205.2 200.0 196.4 191.0 | VEL 0UT 190.8 194.4 192.7 182.2 171.2 169.3 167.8 155.5 152.8 | MERI IN 175.7 180.0 177.1 177.9 176.7 176.8 178.1 176.4 172.2 | D VEL 0UT 167.2 174.4 175.4 173.4 169.1 169.3 166.5 153.6 | TANG VEL IN OUT -0.0 73.3 0.0 74.8 -0.0 76.6 -0.0 86.5 0.0 97.0 0.0 104.9 -0.0 113.3 0.0 111.7 -0.0 112.6 | WHEEL SPEED IN OUT 165.4 165.3 160.7 160.7 156.3 156.4 141.8 142.6 122.3 123.8 104.1 105.8 91.0 92.3 86.4 87.4 82.6 83.1 |
| RP 1 2 3 4 5 6 7 8 9 | ABS MACH NO IN OUT 0.530 0.540 0.544 0.563 0.535 0.568 0.538 0.577 0.534 0.581 0.535 0.596 0.539 0.603 0.533 0.567 0.520 0.560 | REL M. IN 0.728 0.729 0.713 0.688 0.650 0.620 0.605 0.594 0.577 | ACH NO OUT 0.564 0.577 0.572 0.542 0.510 0.503 0.465 0.456 | MERID M IN 0.530 0.544 0.535 0.538 0.535 0.535 0.533 0.520 | ACH NO OUT 0.495 0.517 0.521 0.516 0.504 0.506 0.499 0.448 | | MERID PEAK SS VEL R MACH NO 0.952 0.728 0.969 0.729 0.990 0.713 0.975 0.688 0.957 0.650 0.957 0.620 0.935 0.605 0.871 0.632 0.871 0.662 |
| RP 23 4 5 6 7 8 9 | PERCENT INC SPAN MEAN 5.00 -0.0 10.00 -1.3 15.00 -1.2 30.00 -2.2 50.00 -2.3 70.00 -2.3 85.00 -0.4 90.00 0.7 95.00 2.3 | | 8.2 9.2 10.3 11.3 11.9 12.1 10.9 11.0 | D-FACT 0.379 0.366 0.361 0.400 0.431 0.417 0.413 0.455 0.449 | EFF 0.971 0.960 0.956 0.942 0.928 0.962 0.907 0.717 0.729 | LOSS COEFF TOT PROF 0.013 0.013 0.019 0.019 0.022 0.022 0.030 0.030 0.038 0.038 0.020 0.020 0.048 0.048 0.141 0.141 0.138 0.138 | LOSS PARAM TOT PROF 0.007 0.007 0.009 0.009 0.011 0.011 0.015 0.015 0.019 0.019 0.009 0.009 0.021 0.021 0.060 0.060 0.057 0.057 |

TABLE VII. - Continued.

(c) 80 Percent of design speed; reading 1640

| RP 1 2 3 4 5 6 7 8 9 | RAD IN 24.729 2 24.026 2 23.322 2 21.173 1 18.321 1 15.540 1 13.541 1 12.906 1 12.289 | 0UT 24.714 24.028 23.343 21.285 18.542 15.799 13.741 | ABS IN 0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 | BETAM 0UT 30.0 28.3 28.6 30.8 33.7 35.6 37.8 39.2 40.2 | REL IN 47.5 45.9 45.8 43.0 39.1 34.6 31.0 30.0 29.3 | BETAM 0UT 31.2 28.1 25.9 19.2 10.2 0.7 -6.6 -8.3 -11.5 | TOTAL IN 288.9 288.9 288.5 288.0 287.9 287.8 287.7 | TEMP RATIO 1.044 1.044 1.046 1.043 1.039 1.035 1.032 1.030 | IN 9.99 10.13 10.14 | PRESS RATIO 1.145 1.147 1.152 1.149 1.136 1.125 1.106 1.084 1.086 |
|----------------------|---|--|--|---|--|--|--|--|---|---|
| RP 1 25 4 5 6 7 8 9 | ABS IN 151.7 156.5 152.5 153.0 151.3 151.2 151.6 150.0 146.8 | VEL 0UT 161.9 170.8 173.5 176.6 177.5 169.1 169.3 | REL IN 224.8 224.9 218.7 209.1 194.9 183.6 176.9 173.2 168.3 | YEL 0UT 163.9 170.5 169.3 160.7 149.0 145.6 141.3 132.5 132.0 | MERI IN 151.7 156.5 152.5 153.0 151.3 151.2 151.6 150.0 146.8 | D VEL 0UT 140.2 150.4 152.4 151.8 146.7 145.6 140.3 131.1 129.3 | TANO !N 0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 | VEL 0UT 80.9 81.1 82.9 90.3 97.9 104.3 108.7 106.8 109.3 | WHEEL IN 165.8 161.4 156.7 142.5 122.9 104.2 91.1 86.6 82.4 | SPEED 0UT 165.7 161.4 156.8 143.2 124.3 106.0 92.5 87.6 83.0 |
| RP 1 2 3 4 5 6 7 8 9 | ABS MA IN 0.454 0.469 0.457 0.459 0.454 0.455 0.450 0.440 | OUT 0.475 0.503 0.511 0.522 0.522 0.532 0.528 0.502 0.503 | REL M. IN 0.673 0.674 0.656 0.628 0.585 0.551 0.531 0.520 0.505 | OUT 0.481 0.502 0.499 0.475 0.442 0.432 0.432 0.432 0.393 0.393 | MERID M (N 0.454 0.469 0.457 0.459 0.454 0.453 0.455 0.450 0.440 | ACH NO OUT 0.412 0.443 0.449 0.445 0.435 0.432 0.417 0.389 0.384 | | | | PEAK SS MACH NG 0.827 0.789 0.775 0.718 0.666 0.623 0.638 0.645 0.654 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 | INCI MEAN 4.3 2.8 3.1 2.2 2.1 2.0 3.6 4.6 | DENCE | DEV 10.5 11.1 11.7 12.7 13.1 12.5 11.4 | D-FACT 0.472 0.441 0.432 0.460 0.488 0.476 0.475 0.503 | EFF 0.896 0.901 0.900 0.942 0.961 0.970 0.907 0.769 | LOSS CO TOT 0.058 0.056 0.061 0.036 0.024 0.019 0.058 0.141 | DEFF PROF 0.058 0.056 0.061 0.036 0.024 0.019 0.058 0.141 | LOSS PATOT 0.028 0.027 0.030 0.018 0.012 0.009 0.026 0.060 | ARAM PROF 0.028 0.027 0.030 0.018 0.012 0.009 0.026 0.060 |

(d) 80 Percent of design speed; reading 1641

| RP 1 2 3 4 5 6 7 8 9 | RAD I IN 24.729 2 24.026 2 23.322 2 21.173 2 18.321 1 15.540 1 12.906 1 12.289 1 | 0UT 24.714 24.028 23.343 21.285 18.542 15.799 13.741 | ABS [N -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 | BETAM OUT 35.9 33.5 34.0 36.5 38.2 40.0 41.0 42.2 | REL IN 50.8 48.9 48.7 45.9 41.9 37.8 34.1 33.0 32.3 | BETAM OUT 31.9 29.1 26.6 19.2 10.1 0.9 -5.9 -7.9 -11.5 | TOTA IN 288.8 288.7 288.5 288.1 288.0 287.8 287.8 287.8 | RATIO 1.050 1.048 1.049 1.045 1.040 1.036 1.031 1.029 1.030 | TOTAL IN 10.01 10.13 10.14 10.15 10.14 10.14 10.14 | PRESS RATIO 1.149 1.146 1.151 1.154 1.141 1.125 1.101 1.088 1.090 |
|----------------------|---|--|--|--|--|--|--|---|---|---|
| RP 1 2 5 4 5 6 7 8 9 | ABS IN 136.1 141.1 138.2 138.0 136.9 134.7 134.0 133.1 130.6 | VEL 0UT 153.0 159.3 163.0 168.7 168.5 163.4 158.6 159.4 | REL IN 215.4 214.8 209.4 198.3 184.0 170.5 161.8 158.7 154.4 | VEL 0UT 145.9 152.1 152.5 148.2 137.8 132.4 125.9 120.8 120.6 | MERIL IN 136.1 141.1 138.2 138.0 136.9 134.7 134.0 133.1 130.6 | D VEL 0UT 123.9 132.8 136.4 140.0 135.7 132.4 125.3 119.6 118.2 | TAN IN -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.0 | G VEL OUT 89.8 88.0 89.2 94.2 100.3 104.2 105.0 104.1 | WHEEL IN 167.0 162.0 157.2 142.3 123.0 104.4 90.7 86.5 82.4 | SPEED 0UT 166.9 162.0 157.4 143.0 124.4 106.2 92.0 87.5 83.0 |
| RP 1 2 3 4 5 6 7 8 9 | ABS MAIN 0.406 0.422 0.413 0.413 0.409 0.403 0.400 0.398 0.390 | OUT 0.447 0.467 0.478 0.497 0.498 0.499 0.484 0.470 0.472 | REL M. IN 0.643 0.642 0.625 0.550 0.550 0.483 0.474 0.461 | ACH NO OUT 0,426 0.445 0.447 0.437 0.407 0.392 0.373 0.358 0.357 | MERID M IN 0.406 0.422 0.413 0.413 0.409 0.403 0.400 0.398 0.390 | ACH NO OUT 0.362 0.389 0.400 0.412 0.401 0.392 0.371 0.354 0.350 | | | | PEAK SS MACH NO 0.867 0.828 0.809 0.748 0.691 0.643 0.637 0.641 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INCII MEAN 7.5 5.9 6.0 5.1 5.0 5.2 6.7 7.6 9.0 | DENCE | DEV 11.3 12.1 12.4 12.7 12.9 12.7 12.1 10.5 | D-FACT 0.555 0.518 0.504 0.504 0.526 0.513 0.511 0.524 0.512 | EFF 0.813 0.823 0.839 0.924 0.959 0.952 0.897 0.824 0.827 | LOSS C TOT 0.127 0.117 0.112 0.054 0.029 0.036 0.073 0.123 0.130 | OEFF PROF 0.127 0.117 0.112 0.054 0.029 0.036 0.073 0.123 0.130 | LOSS P TOT 0.060 0.056 0.055 0.027 0.015 0.017 0.032 0.053 | ARAM PROF 0.060 0.056 0.055 0.027 0.015 0.017 0.032 0.053 0.054 |

TABLE VII. - Continued.

(e) 80 Percent of design speed; reading 1642

| RP 1 2 3 4 5 6 7 8 9 | RADII IN 0U 24.729 24.7 24.026 24.02 23.322 23.3 21.173 21.28 18.321 18.5 15.540 15.7 13.541 13.7 12.906 13.0 12.289 12.3 | IN -0.0 28 0.0 35 -0.0 85 -0.0 42 0.0 99 -0.0 | BETAM OUT 50.7 45.9 43.2 37.2 39.4 40.1 40.8 41.7 42.8 | REL IN 54.9 53.1 52.7 49.7 45.9 41.2 37.5 36.4 35.5 | BETAM 0UT 31.2 28.9 26.8 19.3 9.3 0.7 -5.6 -8.0 -11.5 | TOTA IN 288.7 288.7 288.3 288.1 288.0 287.9 287.9 287.9 | L TEMP RATIO 1.057 1.053 1.051 1.047 1.042 1.036 1.031 1.030 | IN 10.05 10.13 10.14 10.14 | PRESS RATIO 1.141 1.132 1.132 1.152 1.152 1.143 1.123 1.102 1.094 1.094 |
|---|---|--|--|--|--|---|---|--|--|
| RP - 234567-89 | ABS VEL IN 001117.1 143.121.3 146.119.6 161.119.6 164.119.0 162.118.6 159.117.6 156.115.6 156. | IN 7 203.6 6 202.0 0 197.2 7 186.3 2 171.8 2 158.2 2 149.5 6 146.1 | VEL 0UT 106.3 116.6 121.8 136.5 128.6 124.2 121.0 118.0 117.4 | MER1 IN 117.1 121.3 119.6 120.6 119.6 119.0 118.6 117.6 | D VEL 0UT 90.9 102.1 108.7 128.9 127.0 124.1 120.4 116.8 115.0 | TAN IN -0.0 0.0 -0.0 -0.0 -0.0 -0.0 -0.0 | G VEL OUT 111.2 105.2 101.9 97.7 104.1 104.4 104.1 104.3 | WHEEL IN 166.5 161.5 156.7 142.1 123.3 104.2 91.0 86.8 82.6 | SPEED OUT 166.4 161.5 156.9 142.8 124.8 106.0 92.3 87.8 83.1 |
| RP 1 2 3 4 5 6 7 8 9 | ABS MACH N 1N OUT 0.348 0.41 0.361 0.42 0.356 0.43 0.359 0.47 0.356 0.48 0.354 0.47 0.353 0.46 0.350 0.46 | 1 N 7 0.605 27 0.601 35 0.586 75 0.555 84 0.511 79 0.471 71 0.445 83 0.435 | ACH NO OUT 0.309 0.340 0.356 0.401 0.379 0.367 0.358 0.349 0.347 | MERID M IN 0.348 0.361 0.356 0.359 0.356 0.354 0.353 0.350 0.344 | ACH NO OUT 0.264 0.297 0.317 0.378 0.374 0.367 0.356 0.346 0.340 | | | | PEAK SS MACH NO 0.901 0.863 0.841 0.776 0.715 0.653 0.640 0.639 |
| RP 1 2 3 4 5 6 7 8 9 | SPAN ME 5.00 10 10.00 10 15.00 10 30.00 5 70.00 8 85.00 10 90.00 11 | NCIDENCE AN 1.6 0.0 0.0 0.0 0.0 0.0 0.0 0.1 1.0 2.3 | DEV 10.6 11.8 12.6 12.7 12.1 12.5 12.5 12.0 | D-FACT 0.783 0.711 0.664 0.545 0.557 0.528 0.501 0.503 0.491 | 0.679 0.684 0.705 0.875 0.936 0.942 0.905 0.859 0.857 | LOSS C TOT 0.268 0.251 0.238 0.104 0.054 0.050 0.079 0.119 | 0EFF PR0F 0.268 0.251 0.238 0.104 0.054 0.050 0.079 0.119 0.126 | LOSS P TOT 0.128 0.121 0.115 0.052 0.027 0.023 0.035 0.051 0.052 | ARAM PROF 0.128 0.121 0.115 0.052 0.027 0.023 0.035 0.051 0.052 |

(f) 90 Percent of design speed; reading 1636

| RP 1 2 3 4 5 6 7 8 9 | RADII IN 0 24.729 24. 24.026 24. 23.322 23. 21.173 21. 18.321 18. 15.540 15. 13.541 13. 12.906 13. 12.289 12. | OUT IN 714 0.0 028 0.0 343 0.0 285 0.0 542 0.0 799 0.0 741 0.0 056 0.0 | BETAM 0UT 24.2 23.0 23.8 26.5 29.3 30.8 33.2 34.8 35.7 | REL (N 39.6 38.7 38.2 35.3 32.8 28.7 25.4 24.7 24.3 | BETAM 0UT 27.3 24.9 22.9 16.0 7.2 -0.3 -6.8 -8.6 -10.4 | TOTAL IN 289.3 289.0 288.7 288.1 287.7 287.7 287.7 287.6 287.6 | TEMP RATIO 1.054 1.054 1.054 1.051 1.046 1.041 1.038 1.036 | TOTAL IN 10.20 10.30 10.31 10.31 9.96 9.97 9.97 9.95 9.89 | PRESS RATIO 1.141 1.155 1.152 1.152 1.175 1.154 1.127 1.091 1.080 |
|----------------------|---|--|---|--|---|---|---|--|---|
| RP 1 2 3 4 5 6 7 8 9 | 226.0 21 227.6 22 224.0 22 226.0 22 215.4 23 214.6 23 215.5 23 212.0 22 | L REL IN 2.3 293.4 2.8 291.5 3.5 285.1 9.1 276.9 4.3 256.2 244.5 2.7 233.3 5.2 226.3 | VEL .0UT 217.9 226.1 221.9 213.2 205'.9 202.4 196.1 183.4 177.6 | IN 226.0 227.6 224.0 226.0 215.4 214.6 | VEL 0UT 193.6 205.1 204.4 205.0 204.3 202.4 194.7 181.4 174.7 | TAN(IN 0.0 0.0 0.0 0.0 0.0 0.0 0.1 0.1 | VEL 0UT 87.0 86.9 90.3 102.3 114.7 120.5 127.3 126.1 125.6 | WHEEL IN 187.0 182.1 176.4 160.1 138.8 117.3 102.6 97.5 93.0 | SPEED 0UT 186.9 182.1 176.5 160.9 140.5 119.3 104.1 98.7 93.6 |
| RP 23 4 5 6 7 8 9 | 0.694 0. 0.700 0. 0.688 0. 0.696 0. 0.661 0. 0.658 0. 0.661 0. 0.649 0. | REL M WIT IN 630 0.901 664 0.896 667 0.876 686 0.852 705 0.786 711 0.750 703 0.732 665 0.715 647 0.692 | ACH NO OUT 0.647 0.675 0.662 0.638 0.619 0.611 0.593 0.553 | MERID M IN 0.694 0.700 0.688 0.696 0.661 0.658 0.661 0.649 0.631 | OUT | | | | PEAK SS MACH NO 0.901 0.896 0.876 0.786 0.750 0.732 0.715 0.748 |
| RP 1 2 3 4 5 | 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 | INCIDENCE MEAN -3.7 -4.4 -4.4 -5.4 -4.2 -4.0 -2.0 -0.7 1.0 | DEV 6.7 7.9 8.7 9.4 10.1 11.4 11.2 11.4 | D-FACT 0.423 0.389 0.394 0.425 0.422 0.406 0.416 0.449 0.450 | 0.709 0.787 0.769 0.763 0.925 0.906 0.844 0.668 0.621 | LOSS C1 TOT 0.125 0.092 0.103 0.111 0.038 0.046 0.071 0.145 0.165 | 0EFF PROF 0.125 0.092 0.103 0.111 0.038 0.046 0.071 0.145 0.165 | LOSS P TOT 0.062 0.046 0.052 0.056 0.019 0.022 0.031 0.062 0.068 | ARAM PROF 0.062 0.046 0.052 0.056 0.019 0.022 0.031 0.062 0.068 |

(g) 90 Percent of design speed; reading 1637

| RP 1 2 3 4 5 6 7 8 9 | RAD IN 24.729 24.026 23.322 21.173 18.321 15.540 13.541 12.906 12.289 | 0UT 24.714 24.028 23.343 21.285 18.542 15.799 13.741 13.056 | ABS IN 0.0 0.0 0.0 0.0 0.0 0.0 | BETAM OUT 26.4 25.6 25.5 28.3 31.2 33.5 35.7 37.3 38.3 | REL IN 44.4 42.7 42.4 39.6 35.7 31.4 27.8 27.0 26.6 | BETAM OUT 29.4 26.7 24.7 18.1 9.3 -0.1 -7.5 -9.1 -11.6 | TOTA IN 289.1 289.0 288.5 288.0 287.9 287.7 287.9 287.8 | RAT10 1.054 1.053 1.055 1.055 1.049 1.046 1.042 1.039 1.038 | IN 9.94 10.13 10.15 10.15 | 1.156 1.136 |
|----------------------|---|---|--|---|---|--|---|---|--|---|
| RP 1 25 4 5 6 7 8 9 | IN 190.0 | VEL 0UT 195.5 203.7 207.1 210.1 211.2 215.7 216.2 205.3 203.1 | REL IN 265.9 266.0 259.6 250.0 235.5 224.0 217.7 213.3 207.1 | VEL 0UT 201.1 205.7 205.7 194.6 183.2 179.9 177.1 165.4 162.6 | MERI 1N 190.0 195.5 191.6 192.7 191.3 191.2 192.5 190.0 185.2 | D VEL 0UT 175.1 183.8 186.8 185.0 180.7 179.9 175.6 163.3 159.3 | TAN IN 0.0 0.0 0.0 0.0 0.0 0.0 0.0 | G VEL OUT 87.0 87.9 89.3 99.6 109.4 118.9 126.1 124.3 125.9 | WHEEL IN 186.0 180.4 175.2 159.3 137.4 116.7 101.5 97.0 92.7 | SPEED 0UT 185.8 180.4 175.3 160.1 139.0 118.7 103.1 98.1 93.3 |
| RP 1 2 5 4 5 6 7 8 9 | ABS MAIN 0.576 0.594 0.581 0.581 0.585 0.577 0.562 | 0.603 0.614 0.625 0.630 0.646 0.648 0.614 0.607 | REL M IN 0.805 0.807 0.788 0.760 0.715 0.681 0.662 0.648 0.628 | ACH NO 0UT 0.593 0.609 0.610 0.579 0.539 0.531 0.495 0.486 | MERID M IN 0.576 0.594 0.581 0.586 0.581 0.585 0.577 0.562 | ACH NC 0UT 0.517 0.544 0.550 0.539 0.539 0.539 0.527 0.489 0.476 | | | | PEAK SS MACH NO 0.875 0.807 0.788 0.760 0.715 0.681 0.690 0.723 0.747 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INCI MEAN 1.1 -0.4 -0.2 -1.2 -1.3 -1.2 0.4 1.6 3.3 | DENCE | 8.8 9.7 10.5 11.5 12.2 11.7 10.6 10:9 | D-FACT 0.426 0.409 0.395 0.432 0.456 0.449 0.444 0.478 | 0.931 | LOSS C TOT 0.036 0.037 0.035 0.041 0.041 0.060 0.136 0.145 | OEFF PROF 0.036 0.037 0.035 0.041 0.041 0.060 0.136 0'.145 | LOSS P TOT 0.017 0.018 0.018 0.018 0.020 0.019 0.027 0.058 0.060 | PROF 0.017 0.018 0.018 0.018 0.020 0.019 0.027 0.058 0.060 |

TABLE VII. - Continued.

(h) 90 Percent of design speed; reading 1632

| RP 1 2 3 4 5 6 7 8 9 | 24.729 24 24.026 24 23.322 23 21.173 21 18.321 18 15.540 15 | OUT .714 .028 .343 .285 .542 .799 .741 | ABS IN 0.0 -0.0 -0.0 0.0 -0.0 -0.0 -0.0 | BETAM OUT 30.7 28.7 28.3 30.8 34.3 36.2 38.2 39.8 40.9 | REL IN 47.2 45.5 45.2 42.4 38.8 34.4 30.9 30.0 29.2 | BETAM OUT 30.9 28.0 25.9 18.7 9.4 0.1 -7.1 -9.2 -12.6 | TOTAL IN 289.2 289.1 288.7 287.9 287.8 287.8 287.7 287.7 | RATIO 1.058 1.058 1.058 1.057 1.052 1.046 1.042 1.040 | TOTAL IN 9.96 10.14 10.14 10.16 10.15 10.15 | PRESS RATIO 1.189 1.189 1.195 1.196 1.180 1.160 1.135 1.111 |
|---|--|--|---|--|---|---|---|--|--|--|
| R - 25456789 | 173.3 1 178.9 1 175.5 1 175.7 2 172.7 2 171.5 2 171.1 1 169.2 1 | CUT 82.7 92.1 96.1 00.5 00.7 01.7 99.4 91.2 | REL IN 255.1 255.2 249.0 237.9 221.6 207.8 199.4 195.4 189.7 | VEL 0UT 183.0 190.9 192.0 181.8 168.1 162.8 157.8 148.7 148.4 | MERII IN 173.3 178.9 175.5 175.7 172.7 171.5 171.1 169.2 165.6 | VEL 0UT 157.1 168.5 172.7 172.2 165.8 162.8 156.6 146.8 | TAN(IN 0.0 -0.0 -0.0 0.0 0.0 -0.0 -0.0 -0.0 - | 93.2 92.3 92.9 102.8 113.1 119.1 123.4 122.5 | WHEEL IN 187.3 182.0 176.7 160.3 138.9 117.5 102.4 97.6 92.5 | SPEED OUT 187.2 182.0 176.8 161.2 140.6 119.4 103.9 98.7 93.1 |
| RP 1 2 3 4 5 6 7 8 9 | 0.522 0 0.540 0 0.530 0 0.531 0 0.521 0 0.518 0 0.517 0 0.511 0 | 0UT .536 .565 .578 .593 .595 .600 .594 | REL M/ IN 0.769 0.770 0.751 0.719 0.669 0.627 0.602 0.589 0.572 | OUT 0.537 0.562 0.566 0.538 0.499 0.485 0.471 0.443 0.442 | MERID MA 1N 0.522 0.540 0.530 0.531 0.521 0.518 0.517 0.511 0.499 | OUT 0.461 0.496 0.509 0.509 0.492 0.485 0.467 0.437 | | | | PEAK SS MACH NO 0.934 0.888 0.869 0.802 0.754 0.704 0.721 0.731 |
| RP 123456789 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 | INCID MEAN 3.9 2.5 2.5 1.7 1.9 1.8 3.5 4.6 5.9 | ENCE | DEV 10.2 11.0 11.7 12.2 12.3 11.9 10.9 10.8 9.3 | D-FACT 0.487 0.452 0.432 0.464 0.499 0.488 0.484 0.511 0.498 | 0.875 0.881 0.896 0.928 0.931 0.936 0.875 0.762 0.771 | LOSS COTOT 0.073 0.069 0.064 0.046 0.046 0.043 0.081 0.151 | OEFF PROF 0.073 0.069 0.064 0.046 0.046 0.043 0.081 0.151 | LOSS P TOT 0.035 0.034 0.031 0.023 0.023 0.023 0.020 0.035 0.064 | ARAM PROF 0.035 0.034 0.031 0.023 0.023 0.020 0.035 0.064 |

(i) 90 Percent of design speed; reading 1633

| RP 1 2 3 4 5 6 7 8 9 | RADI IN 24.729 2 24.026 2 23.322 2 21.173 2 18.321 1 15.540 1 13.541 1 12.906 1 12.289 1 | 0UT 4.714 4.028 3.343 1.285 8.542 5.799 3.741 3.056 | ABS IN 0.0 0.0 0.0 0.0 0.0 0.0 0.0 | BETAM 0UT 35.5 33.4 32.4 33.3 36.7 38.3 40.1 41.4 42.5 | REL 1N 49.7 48.1 47.7 45.0 41.2 37.1 33.5 32.6 31.9 | BETAM OUT 31.7 28.8 26.3 19.3 9.5 0.3 -6.4 -8.9 -12.6 | TOTA IN 289.0 288.9 288.5 287.9 288.0 287.9 287.8 287.6 | L TEMP RATIO 1.062 1.060 1.057 1.052 1.046 1.040 1.039 1.039 | TOTAL IN 9.99 10.13 10.14 10.15 10.15 10.14 10.14 | PRESS RATIO 1.184 1.192 1.196 1.181 1.161 1.129 1.116 1.120 |
|----------------------|--|---|--|--|--|--|--|--|--|---|
| RP 1 2 5 4 5 6 1 8 9 | 162.4 160.1 160.2 157.8 155.7 154.1 152.2 | VEL 0UT 171.7 179.5 184.9 191.0 191.2 191.7 185.6 181.6 182.6 | REL IN 244.3 243.3 238.0 226.5 209.8 195.1 184.8 180.7 175.4 | VEL 0UT 164.4 171.0 174.1 169.1 155.5 150.5 142.9 137.9 137.9 | MER II IN 158.1 162.4 160.1 160.2 157.8 155.7 154.1 152.2 148.9 | VEL 0UT 139.8 149.9 156.1 159.5 153.3 150.5 142.1 136.3 134.5 | TAN IN 0.0 0.0 0.0 0.0 -0.0 0.0 0.0 | G VEL OUT 99.7 98.8 99.1 105.0 114.2 118.7 119.5 120.0 123.5 | WHEEL IN 186.2 181.2 176.1 160.1 138:2 117.7 102.1 97.4 92.7 | SPEED OUT 186.1 181.2 176.3 160.9 139.9 119.6 103.6 98.6 93.4 |
| RP 1 23 4 5 6 7 8 9 | 0.488 0.481 0.482 0.474 0.468 0.463 0.457 | CH NO OUT 0.501 0.526 0.543 0.563 0.565 0.569 0.551 0.539 0.542 | REL M IN 0.733 0.731 0.715 0.681 0.630 0.586 0.555 0.542 0.526 | ACH NO OUT 0.480 0.501 0.511 0.498 0.460 0.447 0.424 0.409 0.409 | MERID M IN 0.474 0.488 0.481 0.482 0.474 0.468 0.463 0.457 0.447 | ACH NO OUT 0.408 0.439 0.458 0.470 0.453 0.447 0.422 0.404 0.399 | | | | PEAK SS MACH NO 0.958 0.920 0.900 0.837 0.774 0.724 0.720 0.726 0.730 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INCII MEAN 6.4 5.1 5.1 4.3 4.3 4.4 6.1 7.2 8.6 | DENCE | DEV 11.1 11.8 12.1 12.8 12.4 12.1 11.7 11.1 9.3 | D-FACT 0.555 0.521 0.495 0.499 0.533 0.517 0.515 0.525 | EFF 0.799 0.824 0.852 0.912 0.943 0.950 0.874 0.814 0.833 | LOSS C TOT 0.134 0.115 0.101 0.063 0.042 0.037 0.090 0.135 0.128 | OEFF PROF 0.134 0.115 0101 0.063 0.042 0.037 0.090 0.135 0.128 | LOSS P TOT 0.064 0.056 0.049 0.031 0.021 0.017 0.040 0.058 0.053 | ARAM PROF 0.064 0.056 0.049 0.031 0.021 0.017 0.040 0.058 0.053 |

(j) 90 Percent of design speed; reading 1634

| RP 1 2 3 4 5 6 7 8 9 | RADII IN OUT 24.729 24.714 24.026 24.028 23.322 23.343 21.173 21.285 18.321 18.542 15.540 15.799 13.541 13.741 12.906 13.056 12.289 12.370 | ABS BETAM IN OUT 0.0 44.8 0.0 40.5 0.0 38.2 0.0 36.1 0.0 38.5 0.0 39.6 0.0 41.1 0.0 42.1 0.0 43.2 | REL BETAM IN OUT 52.8 31.5 51.3 29.6 50.6 26.9 47.9 19.1 44.1 9.3 39.7 0.6 36.2 -6.2 35.1 -8.6 34.3 -12.3 | TOTAL TEMP IN RATIO 288.9 1.067 288.8 1.064 288.4 1.064 287.9 1.054 287.8 1.046 287.9 1.040 287.8 1.039 287.7 1.039 | TOTAL PRESS IN RATIO 10.01 1.182 10.13 1.175 10.14 1.180 10.14 1.196 10.15 1.184 10.14 1.159 10.14 1.129 10.13 1.119 10.11 1.122 |
|----------------------|---|---|--|---|---|
| RP 1 23 4 15 67: 8 9 | ABS VEL IN OUT 141.6 164.0 146.2 168.6 145.0 174.0 144.4 184.4 143.0 186.6 141.2 184.8 140.1 180.6 138.7 177.2 136.4 178.3 | REL VEL IN OUT 234.5 136.4 233.7 147.4 228.6 153.3 215.2 157.7 199.0 148.0 183.6 142.3 173.6 136.9 169.6 133.1 | MERID VEL IN OUT 141.6 116.3 146.2 128.1 145.0 136.7 144.4 149.0 143.0 146.0 141.2 142.3 140.1 136.1 138.7 131.5 136.4 130.0 | TANG VEL IN OUT 0.0 115.5 0.0 109.5 0.0 107.5 0.0 108.7 0.0 116.1 0.0 117.8 0.0 118.8 0.0 118.7 0.0 122.0 | WHEEL SPEED IN OUT 186.9 186.8 182.4 182.4 176.8 176.9 159.6 160.4 138.4 140.1 117.4 119.3 102.4 103.9 97.6 98.7 92.9 93.6 |
| RP: 23456789 | ABS MACH NO IN OUT 0.423 0.476 0.437 0.491 0.434 0.508 0.432 0.542 0.428 0.550 0.423 0.547 0.419 0.535 0.415 0.525 0.408 0.529 | REL MACH NO IN OUT 0.700 0.396 0.699 0.429 0.684 0.448 0.644 0.463 0.596 0.436 0.549 0.421 0.519 0.406 0.507 0.394 0.493 0.395 | MERID MACH NO IN OUT 0.423 0.338 0.437 0.373 0.434 0.399 0.432 0.438 0.428 0.431 0.423 0.421 0.419 0.403 0.415 0.390 0.408 0.386 | | MERID PEAK SS VEL R MACH NO 0.822 0.994 0.877 0.960 0.943 0.933 1.032 0.860 1.021 0.795 1.008 0.733 0.971 0.723 0.948 0.723 0.953 0.725 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT INC SPAN MEAN 5.00 9.6 10.00 8.2 15.00 8.0 30.00 7.1 70.00 7.1 70.00 7.1 85.00 8.8 90.00 9.7 95.00 11.0 | | D-FACT EFF 0.693 0.732 0.628 0.731 0.585 0.756 0.534 0.878 0.551 0.921 0.529 0.933 0.516 0.877 0.520 0.836 0.506 0.865 | LOSS COEFF TOT PROF 0.206 0.206 0.200 0.200 0.188 0.188 0.099 0.099 0.066 0.066 0.056 0.056 0.099 0.099 0.133 0.133 0.114 0.114 | LOSS PARAM TOT PROF 0.098 0.098 0.096 0.096 0.091 0.091 0.049 0.049 0.033 0.033 0.026 0.026 0.043 0.043 0.057 0.057 0.047 0.047 |

TABLE VII. - Continued.

(k) 100 Percent of design speed; reading 1625

| RP 1 23 4 5 6 7 8 9 | 15.540 | 0UT 24.714 24.028 23.343 21.285 18.542 15.799 13.741 13.056 | ABS IN -0.0 0.0 -0.0 -0.0 -0.0 -0.0 -0.0 | BETAM 0UT 28.3 25.8 26.4 28.8 31.5 33.7 36.6 38.0 38.6 | REL IN 44.0 42.4 42.1 39.1 35.3 31.2 28.0 27.2 26.7 | BETAM 0UT 29.5 26.4 24.3 17.1 8.6 -0.3 -7.6 -9.3 -11.5 | TOTA IN 289:3 289:0 288:6 288:0 287:8 287:8 287:8 287:6 | RATIO 1.070 1.069 1.071 1.069 1.063 1.058 1.051 1.048 | TOTAL IN 9.89 10.15 10.15 10.16 10.16 10.16 | PRESS RATIO 1.216 1.228 1.230 1.234 1.215 1.197 1.161 1.127 |
|----------------------|---|--|--|---|--|--|---|---|---|---|
| R 1 234568 89 | ABS IN 215.6 221.0 217.1 219.4 218.0 215.9 214.8 211.2 206.0 | VEL 0UT 213.7 228.9 231.7 238.4 239.5 241.9 236.2 225.5 224.6 | REL IN 299.6 299.4 292.8 282.6 267.1 252.5 243.2 237.4 230.6 | VEL 0UT 216.4 230.0 227.8 218.6 206.6 201.2 191.2 180.1 179.2 | MERI IN 215.6 221.0 217.1 219.4 218.0 215.9 214.8 211.2 206.0 | VEL 0UT 188.3 206.1 207.6 208.9 204.3 201.2 189.6 177.7 175.5 | TAN IN -0.0 0.0 -0.0 -0.0 -0.0 -0.0 0.0 | G VEL OUT 101.2 99.7 102.9 114.8 125.1 134.2 140.9 138.8 140.1 | WHEEL IN 208.0 201.9 196.5 178.2 154.2 131.0 114.0 108.5 | SPEED OUT 207.9 201.9 196.7 179.1 156.1 133.2 115.7 109.8 104.3 |
| RP 1 2 3 4 5 6 7 8 9 | ABS M 1N 0.659 0.678 0.665 0.669 0.662 0.659 0.659 | ACH NO OUT 0.629 0.679 0.688 0.711 0.717 0.727 0.711 0.677 0.674 | REL M IN 0.916 0.918 0.897 0.868 0.820 0.774 0.746 0.727 0.705 | ACH NO OUT 0.637 0.682 0.676 0.652 0.619 0.605 0.576 0.541 | MERID M IN 0.659 0.678 0.665 0.665 0.669 0.662 0.659 0.646 0.629 | ACH NO OUT 0.554 0.611 0.616 0.623 0.612 0.605 0.571 0.533 0.527 | | | | PEAK SS MACH NG 0.974 0.918 0.897 0.868 0.820 0.774 0.786 0.817 0.842 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INCI MEAN 0.7 -0.6 -0.5 -1.6 -1.7 -1.4 0.6 1.8 3.4 | DENCE | DEV 8.9 9.3 10.1 10.6 11.5 11.5 10.4 10.7 | D-FACT 0.466 0.416 0.413 0.441 0.462 0.455 0.472 0.496 0.480 | EFF 0.818 0.872 0.859 0.901 0.908 0.908 0.908 0.851 0.727 0.723 | LOSS C TOT 0.099 0.069 0.057 0.053 0.054 0.082 0.145 0.156 | OEFF PROF 0.099 0.069 0.079 0.057 0.053 0.054 0.082 0.145 0.156 | LOSS F TOT 0.048 0.034 0.039 0.029 0.026 0.025 0.036 0.062 | PROF 0.048 0.034 0.039 0.029 0.026 0.025 0.036 0.062 |

(ℓ) 100 Percent of design speed; reading 1626

| RP 1 2 3 4 5 6 7 8 9 | RAD IN 24.729 24.026 23.322 21.173 18.321 15.540 13.541 12.906 12.289 | 0UT 24.714 24.028 23.343 21.285 18.542 15.799 13.741 13.056 | ABS IN 0.0 0.0 0.0 -0.0 -0.0 0.0 -0.0 | BETAM 0UT 30.6 28.4 28.6 30.9 34.0 35.8 38.1 39.6 40.3 | REL IN 46.2 44.5 44.1 41.2 37.4 33.1 29.7 28.9 28.4 | BETAM 0UT 30.3 27.7 25.2 18.2 9.2 -0.4 -7.4 -9.5 -12.0 | TOTA IN 289.2 289.0 288.6 287.8 287.7 287.8 287.8 287.7 | L TEMP RATIO 1.072 1.072 1.073 1.069 1.064 1.057 1.052 1.049 | TOTAL IN 9.89 10.13 10.15 10.16 10.15 10.15 10.15 | PRESS RATIO 1.243 1.238 1.244 1.246 1.221 1.202 1.164 1.136 1.138 |
|---|---|---|--|---|--|--|--|---|--|---|
| RP 1 2 3 4 5 6 7 8 9 | ABS IN 200.3 206.3 202.9 204.4 202.6 200.5 200.3 197.5 192.6 | VEL 0UT 206.1 216.2 220.5 226.2 226.1 229.9 225.4 216.6 216.0 | REL IN 289.2 289.0 282.4 271.6 255.1 239.5 230.7 225.5 218.8 | VEL 0UT 205.5 214.7 214.0 204.3 189.8 186.5 178.8 169.2 168.5 | MERII 1N 200.3 206.3 202.9 204.4 202.6 200.5 200.3 197.5 192.6 | VEL 0UT 177.4 190.2 193.6 194.1 187.4 186.5 177.4 166.8 164.8 | TAN IN 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0. | G VEL 0UT 104.8 105.5 116.1 126.5 134.5 139.0 138.1 139.7 | WHEEL IN 208.7 202.4 1.96.5 1.78.8 1.54.9 1.30.9 1.14.4 1.08.9 1.04.0 | SPEED OUT 208.5 202.5 196.7 179.8 156.8 133.1 116.1 110.2 |
| RP 1 2 3 4 5 6 7 8 9 | ABS M. IN 0.609 0.629 0.618 0.624 0.618 0.611 0.611 0.601 | 0.605 0.637 0.651 0.671 0.673 0.688 0.675 0.647 | REL M IN 0.879 0.881 0.860 0.829 0.778 0.730 0.703 0.665 | 0.603 0.633 0.632 0.606 0.565 0.558 0.536 0.504 | MERID M 1N 0.609 0.629 0.618 0.624 0.611 0.611 0.601 0.585 | ACH NO 0UT 0.521 0.560 0.572 0.576 0.558 0.558 0.531 0.499 0.493 | | | | PEAK SS MACH NO 1.030 0.973 0.950 0.869 0.815 0.768 0.806 0.822 0.838 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INC II MEAN 2.9 1.4 1.4 0.5 0.4 0.5 2.3 3.5 | DENCE | 9.7 10.6 11.0 11.6 12.0 11.4 10.6 10.5 | D-FACT 0.492 0.454 0.446 0.474 0.506 0.488 0.493 0.516 0.500 | EFF 0.889 0.873 0.884 0.932 0.924 0.943 0.859 0.760 0.776 | LOSS C TOT 0.066 0.075 0.071 0.042 0.048 0.036 0.086 0.143 0.139 | OEFF PROF 0.066 0.075 0.071 0.042 0.048 0.036 0.086 0.143 0.139 | LOSS F TOT 0.032 0.037 0.035 0.021 0.024 0.017 0.038 0.061 0.057 | PROF 0.032 0.037 0.035 0.021 0.024 0.017 0.038 0.061 0.057 |

TABLE VII. - Continued.

(m) 100 Percent of design speed; reading 1627

| RP 1 2 3 4 5 6 7 8 9 | RAD IN 24.729 2 24.026 2 23.322 2 21.173 1 18.321 1 15.540 1 13.541 1 12.906 1 12.289 | 0UT 24.714 24.028 23.343 21.285 18.542 15.799 13.741 13.056 | ABS IN 0.0 -0.0 -0.0 0.0 0.0 0.0 -0.0 | BETAM OUT 34.4 32.0 31.3 33.0 36.0 37.4 39.6 40.9 41.6 | REL IN 48.7 46.9 46.4 43.5 39.7 35.3 31.6 30.8 30.1 | BETAM 0UT 31.7 29.0 26.4 18.9 9.5 -0.2 -7.2 -9.3 -12.5 | TOTAL TEMP IN RATIO 289.1 1.076 289.0 1.074 288.7 1.074 287.9 1.071 287.8 1.065 287.8 1.058 287.8 1.052 288.0 1.049 287.8 1.049 | TOTAL PRESS IN RATIO 9.92 1.240 10.13 1.233 10.15 1.242 10.15 1.251 10.16 1.226 10.15 1.205 10.15 1.162 10.14 1.141 10.10 1.147 |
|----------------------|---|---|---|---|--|--|---|---|
| RP 1 23 4 5 6 7 8 9 | ABS IN 184.0 189.9 187.5 188.7 186.9 185.3 185.7 185.4 179.1 | VEL 0UT 194.7 202.9 209.0 216.8 216.8 220.4 214.7 208.7 209.7 | REL IN 278.7 277.8 272.1 260.3 242.7 227.0 218.1 213.5 207.0 | VEL 0UT 188.8 196.6 199.3 192.2 177.7 175.0 166.7 160.0 | MERII IN 184.0 189.9 187.5 188.7 186.9 185.3 185.7 183.4 179.1 | VEL 0UT 160.6 172.0 178.5 181.8 175.3 175.0 165.4 157.8 156.9 | TANG VEL IN OUT 0.0 110.0 -0.0 107.6 -0.0 108.6 0.0 118.0 0.0 127.5 0.0 133.9 -0.0 136.5 0.0 139.1 | WHEEL SPEED IN OUT 209.3 209.2 202.8 202.8 197.1 197.3 180.2 154.9 156.8 131.2 133.4 114.4 116.1 109.3 110.6 103.7 104.4 |
| RP 1 2 3 4 5 6 7 8 9 | ABS MAIN 0.556 0.576 0.568 0.567 0.562 0.563 0.555 0.542 | OUT 0.568 0.595 0.614 0.640 0.643 0.657 0.640 0.622 0.625 | REL M. IN 0.843 0.842 0.824 0.790 0.736 0.688 0.661 0.647 0.626 | ACH NO OUT 0.551 0.576 0.586 0.568 0.527 0.522 0.497 0.477 | MERID M IN 0.556 0.576 0.568 0.573 0.567 0.562 0.563 0.555 0.542 | ACH NO OUT 0.469 0.504 0.524 0.537 0.520 0.521 0.493 0.470 0.468 | | MERID PEAK SS VEL R MACH NO 0.873 1.071 0.906 1.020 0.952 0.996 0.964 0.923 0.938 0.857 0.945 0.800 0.891 0.811 0.861 0.822 0.876 0.828 |
| RP : 23 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INCI MEAN 5.4 3.8 2.8 2.7 2.7 4.2 5.4 6.8 | DENCE | DEV 11.1 11.9 12.2 12.3 12.3 11.6 10.8 10.7 9.5 | D-FACT 0.543 0.506 0.485 0.501 0.533 0.509 0.515 0.529 0.508 | 0.835 0.837 0.864 0.925 0.923 0.939 0.845 0.786 0.808 | LOSS COEFF TOT PROF 0.108 0.108 0.104 0.104 0.090 0.090 0.052 0.052 0.054 0.054 0.043 0.043 0.104 0.104 0.141 0.141 0.135 0.135 | LOSS PARAM TOT PROF 0.051 0.051 0.050 0.050 0.044 0.044 0.026 0.026 0.027 0.027 0.020 0.020 0.046 0.046 0.060 0.060 0.055 0.055 |

(n) 100 Percent of design speed; reading 1628

| RP 1 2 3 4 5 6 7 8 9 | RADII IN 0 24.729 24. 24.026 24. 23.322 23. 21.173 21. 18.321 18. 15.540 15. 13.541 13. 12.906 13. 12.289 12. | UT IN 714 0.0 028 0.0 343 0.0 285 0.0 542 0.0 799 0.0 741 0.0 056 0.0 | BETAM OUT 39.4 35.1 34.8 34.5 37.6 38.4 40.5 41.4 42.3 | REL IN 50.7 48.8 48.5 45.6 41.6 37.1 33.4 32.3 31.6 | BETAM 0UT 32.1 29.7 26.8 19.7 9.8 0.3 -6.7 -8.8 -12.4 | TOTAL IN 289.0 288.9 288.6 288.0 287.9 287.8 287.8 287.7 | TEMP RATIO 1.078 1.076 1.075 1.072 1.065 1.058 1.051 1.048 | TOTAL IN 9.95 10.13 10.15 10.15 10.15 10.15 10.15 | PRESS RATIO 1.235 1.229 1.236 1.248 1.225 1.205 1.162 1.143 1.151 |
|----------------------|---|--|---|--|---|---|---|---|---|
| RP 1 2 3 4 5 6 7 8 9 | 171.1 18 177.4 19 174.7 20 175.4 20 174.2 20 173.4 21 173.9 20 172.1 20 | L REL IN 6.6 270.0 4.9 269.5 0.2 263.5 9.3 250.8 9.5 232.9 3.3 217.5 7.7 208.3 2.0 203.6 4.3 197.8 | VEL 0UT 170.3 183.4 184.1 183.3 168.4 167.1 158.9 153.4 154.6 | MERII IN 171.1 177.4 174.7 175.4 174.2 173.4 173.9 172.1 168.4 | VEL 0UT 144.3 159.4 164.3 172.6 166.0 167.1 157.8 151.6 151.0 | IN 0.0 | VEL 0UT 118.4 112.1 114.3 118.5 127.8 132.6 134.9 133.6 137.6 | WHEEL IN 208.9 202.9 197.2 179.3 154.6 131.2 114.8 108.8 103.8 | SPEED OUT 208.8 202.9 197.4 180.2 156.5 133.4 116.5 110.1 104.5 |
| RP 1 2 3 4 5 6 7 8 9 | 0.515 0.0 0.535 0.0 0.527 0.0 0.530 0.0 0.526 0.0 0.524 0.0 0.525 0.0 | NO REL M UT IN 543 0.813 569 0.813 586 0.795 616 0.758 620 0.703 634 0.657 618 0.629 601 0.615 608 0.597 | ACH NO 0UT 0.495 0.536 0.539 0.540 0.498 0.497 0.473 0.456 | MERID M 1N 0.515 0.535 0.527 0.530 0.526 0.524 0.525 0.525 0.520 | 0.420 0.465 0.481 0.508 0.491 0.497 0.470 0.449 | | | | PEAK SS MACH NO 1.093 1.046 1.022 0.949 0.874 0.812 0.814 0.816 0.822 |
| RP ! 23 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INCIDENCE MEAN 7.4 5.8 5.8 4.9 4.6 4.5 6.0 6.9 8.4 | DEV 11.4 12.6 12.6 13.1 12.6 12.0 11.3 11.2 9.6 | D-FACT 0.614 0.549 0.537 0.519 0.553 0.521 0.526 0.532 0.513 | EFF 0.798 0.801 0.828 0.902 0.926 0.947 0.860 0.803 0.831 | LOSS COTOT 0.143 0.137 0.122 0.073 0.056 0.040 0.101 0.140 0.129 | 0EFF PROF 0.143 0.137 0.122 0.073 0.056 0.040 0.101 0.140 0.129 | LOSS P. TOT 0.067 0.066 0.059 0.036 0.028 0.019 0.044 0.060 0.053 | PROF 0.067 0.066 0.059 0.036 0.028 0.019 0.044 0.060 0.053 |

TABLE VII. - Concluded.

(o) 100 Percent of design speed; reading 1629

| RP 1 2 3 4 5 6 7 8 9 | RAD IN 24.729 24.026 23.322 21.173 18.321 15.540 13.541 12.906 12.289 | 0UT 24.714 24.028 23.343 21.285 18.542 15.799 13.741 | IN 0.0 0.0 -0.0 -0.0 | BETAM 0UT 48.1 42.3 39.6 36.4 38.6 39.3 40.6 41.9 42.6 | IN 52.9 51.2 50.8 47.8 43.8 39.2 35.3 | BETAM OUT 32.3 29.2 27.0 19.0 9.3 0.1 -6.4 -8.9 -12.0 | | 9.98 10.12 10.15 10.15 10.14 110.15 110.14 1 | RATIO 1.213 1.209 1.212 1.244 1.229 1.204 1.165 |
|----------------------|---|---|---|--|--|---|---|--|--|
| R 1 25456789 | IN 157.9 163.2 160.9 162.1 161.6 161.1 161.8 160.4 | VEL 0UT 179.1 187.0 191.5 206.7 208.9 210.4 205.4 200.5 201.9 | 254.5 241.5 224.0 207.9 198.3 194.1 | VEL 0UT 141.6 158.2 165.5 176.1 165.4 162.9 156.9 150.9 | IN 157.9 163.2 160.9 162.1 161.6 161.1 | VEL OUT 119.7 138.2 147.5 166.5 163.2 162.9 155.9 149.1 148.6 | TANG VEL [N OUT 0.0 133.2 0.0 125.9 0.0 122.2 -0.0 122.5 0.0 130.3 0.0 133.3 0.0 133.8 -0.0 134.0 0.0 136.6 | [N 209.0 2 203.0 2 197.2 1 179.0 1 155.1 1 131.5 1 114.6 1 | OUT 208.9 203.1 197.3 180.0 157.0 133.7 |
| RP 1 2 3 4 5 6 7 8 9 | IN 0.474 0.490 0.484 0.488 0.486 0.485 | 0.518 0.543 0.558 0.608 0.617 0.625 0.611 0.596 0.600 | REL MA IN 0.786 0.783 0.765 0.727 0.674 0.625 0.597 0.584 0.569 | OUT 0.410 0.460 0.482 0.518 0.488 0.484 0.467 0.449 0.452 | 0.484 0.488 0.486 0.485 | 0.442 0.442 0.443 0.443 0.442 | | 0.847 1 0.916 1 1.027 0 1.010 0 1.011 0 0.964 0 | ACH NO 1,118 1.073 1.047 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | MEAN 9.6 | | DEV 11.7 12.1 12.8 12.5 12.1 11.9 11.6 11.1 9.9 | | 0.666 | LOSS COEFF TOT PROF 0.265 0.265 0.229 0.229 0.223 0.223 0.104 0.104 0.069 0.069 0.046 0.046 0.097 0.097 0.143 0.143 0.137 0.137 | 0.125 (0.111 (0.108 (0.052 (0.034 (0.022 (0.042 (0.061 (0. | PROF 0.125 |

TABLE VIII. - BLADE-ELEMENT DATA AT BLADE EDGES FOR STATOR 55

(a) 80 Percent of design speed; reading 1638

| RP 1 23 4 5 6 7 8 9 | RADII IN 25.230 25. 24.547 24. 23.876 24. 21.847 22. 19.164 19. 16.502 17. 14.519 15. 13.858 15. | OUT IN 298 20.7 19.7 298 20.7 19.7 20.5 222 23.3 827 26.7 465 28.6 682 30.2 070 31.8 | -5.4 -5.0 -4.6 -3.6 -3.4 -3.5 -5.0 | IN 20.7 19.7 20.5 23.3 26.7 28.6 30.2 31.8 | BETAM OUT -6.2 -5.4 -5.0 -4.6 -3.6 -3.4 -3.5 -6.5 | TOTAL IN 300.5 300.5 300.4 300.2 299.6 298.5 297.5 296.4 295.8 | RAT10 0.997 0.998 0.999 0.999 1.001 1.004 1.003 1.003 | TOTAL IN 11.40 11.57 11.60 11.63 11.58 11.43 11.18 10.83 | PRESS RATIO 0.945 0.959 0.972 0.980 0.988 0.992 0.986 0.986 |
|---|--|---|--|--|--|--|---|--|---|
| RP 1 2 5 4 5 6 7 8 9 | 201.0 19 208.6 20 210.5 20 217.2 21 221.1 22 221.2 23 214.9 23 202.5 22 | EL REDUT IN 101.6 201.0 | 203.7 209.3 215.8 224.2 231.8 233.6 222.7 | MERII IN 188.0 196.4 197.2 199.4 197.4 194.2 185.8 172.2 163.0 | VEL 0UT 190.4 202.8 208.5 215.1 223.8 231.4 233.1 221.9 212.8 | TAN IN 71.0 70.2 73.6 86.0 99.5 105.8 108.0 106.6 104.2 | G VEL OUT -20.6 -19.2 -18.3 -17.2 -14.1 -13.8 -14.2 -19.4 -24.3 | WHEEL IN 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. | SPEED OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. |
| RP 1 2 3 4 5 6 7 8 9 | 0.599 0. 0.623 0. 0.629 0. 0.651 0. 0.665 0. 0.666 0. 0.647 0. | H NO REL DUT IN 570 0.599 608 0.623 626 0.629 647 0.651 675 0.669 700 0.666 707 0.647 673 0.608 646 0.580 | 0.608 0.626 0.647 0.675 0.700 0.707 0.707 | MERID M 0.560 0.587 0.590 0.598 0.594 0.585 0.559 0.517 0.488 | ACH NO 0UT 0.566 0.606 0.624 0.645 0.673 0.699 0.706 0.670 0.642 | | | | PEAK SS MACH NO 0.599 0.623 0.629 0.651 0.665 0.666 0.647 0.608 0.580 |
| RP 1 2 3 4 5 6 7 8 9 | 10.00 - 15.00 - 30.00 - 50.00 - 70.00 - 85.00 - 90.00 - | INCIDENCE MEAN -19.8 -20.9 -20.1 -17.7 -14.7 -13.2 -12.0 -10.5 -9.8 | DEV 9.5 9.9 10.0 9.5 9.4 8.3 7.5 5.7 | D-FACT 0.358 0.307 0.288 0.287 0.252 0.194 0.138 0.136 0.133 | EFF 0. 0. 0. 0. 0. 0. 0. | LOSS C TOT 0.256 0.177 0.121 0.082 0.045 0.030 0.057 0.063 0.072 | OEFF PROF 0.256 0.177 0.121 0.082 0.045 0.030 0.057 0.063 0.072 | LOSS P TOT 0.174 0.117 0.078 0.049 0.024 0.014 0.023 0.024 0.027 | ARAM PROF 0.174 0.117 0.078 0.049 0.024 0.014 0.023 0.024 0.027 |

TABLE VIII. - Continued.

(b) 80 Percent of design speed; reading 1639

| RP : 23 4 5 6 7 8 9 | RADI IN 25.230 2 24.547 2 23.876 2 21.847 2 19.164 1 16.502 1 14.519 1 13.858 1 13.200 1 | 0UT 5.298 4.671 4.049 2.222 9.827 7.465 5.682 5.070 | ABS IN 23.8 23.2 23.5 26.1 29.3 31.2 33.6 35.3 36.2 | BETAM OUT -5.8 -5.1 -4.8 -4.8 -4.4 -3.7 -3.4 -4.5 -5.5 | REL 1N 23.8 23.2 23.5 26.1 29.3 31.2 33.6 35.3 36.2 | BETAM OUT -5.8 -5.1 -4.8 -4.8 -4.4 -3.7 -3.4 -4.5 -5.5 | TOTA IN 301.0 300.9 300.6 299.7 299.0 298.0 297.6 296.8 296.5 | TEMP RATIO 0.996 0.997 0.998 0.999 1.000 0.999 1.000 | TOTAL IN 11.44 11.61 11.64 11.59 11.47 11.41 11.29 10.96 10.89 | PRESS RATIO 0.968 0.975 0.982 0.993 0.999 0.994 0.988 0.998 |
|----------------------|--|---|---|---|---|---|---|--|--|--|
| R - 234567-89 | 186.0 188.1 191.3 192.0 194.1 193.7 181.8 | VEL 0UT 164.7 174.6 178.5 184.6 187.5 190.4 191.7 184.6 178.4 | REL IN 178.2 186.0 188.1 191.3 192.0 194.1 193.7 181.8 178.6 | VEL 0UT 164.7 174.6 178.5 184.6 187.5 190.4 191.7 184.6 178.4 | MER II IN 163.1 170.9 172.6 171.8 167.4 166.1 161.3 148.3 | VEL OUT 163.9 173.9 177.9 183.9 186.9 190.0 191.4 184.0 177.6 | TAN IN 71.8 73.3 74.9 84.3 93.9 100.4 107.2 105.2 | G VEL OUT -16.8 -15.5 -14.8 -15.3 -14.3 -12.2 -11.2 -17.1 | WHEEL IN 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. | SPEED OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. |
| RP 1 2 3 4 5 6 7 8 9 | 0.551 0.558 0.569 0.572 0.579 0.579 | CH NO 0UT 0.486 0.516 0.528 0.548 0.558 0.568 0.573 0.550 0.531 | REL M. IN 0.526 0.551 0.558 0.569 0.572 0.579 0.579 0.542 0.532 | OUT 0.486 0.516 0.528 0.558 0.558 0.568 0.550 0.531 | MERID M. IN 0.482 0.506 0.512 0.511 0.499 0.496 0.482 0.442 0.429 | OUT 0.483 0.514 0.527 0.546 0.556 0.566 0.572 0.549 0.529 | | | | PEAK SS MACH NC 0.526 0.551 0.558 0.569 0.572 0.579 0.579 0.579 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 | INCII MEAN -16.7 -17.3 -17.1 -14.9 -12.2 -10.7 -8.6 -7.0 -6.2 | DENCE | 9.8 10.2 10.2 9.3 8.6 8.1 7.6 6.2 4.9 | D-FACT 0.414 0.378 0.359 0.343 0.316 0.279 0.251 0.234 0.249 | EFF 0. 0. 0. 0. 0. 0. | LOSS C TOT 0.186 0.137 0.093 0.033 0.006 0.032 0.061 0.011 | OEFF PROF 0.186 0.137 0.093 0.033 0.006 0.032 0.061 0.011 | LOSS F TOT 0.126 0.090 0.060 0.020 0.003 0.014 0.025 0.004 0.020 | PARAM PROF 0.126 0.090 0.060 0.020 0.033 0.014 0.025 0.004 0.020 |

(c) 80 Percent of design speed; reading 1640

| RP 1 2 5 4 15 6 7 8 9 | RADII IN OUT 25.230 25.298 24.547 24.671 23.876 24.049 21.847 22.222 19.164 19.827 16.502 17.465 14.519 15.682 13.858 15.070 13.200 14.448 | ABS BETAM IN OUT 30.0 -3.8 28.3 -3.6 28.4 -3.7 30.3 -3.8 33.1 -3.4 34.9 -2.3 37.0 -2.7 38.4 -3.8 39.4 -5.9 | REL BETAM IN OUT 30.0 -3.8 28.3 -3.6 28.4 -3.7 30.3 -3.8 33.1 -3.4 34.9 -2.3 37.0 -2.7 38.4 -3.8 39.4 -5.9 | TOTAL TEMP IN RATIO 301.6 0.998 301.8 0.997 301.6 0.996 300.4 0.998 299.1 0.999 298.0 0.999 297.1 1.000 296.5 1.000 296.5 0.999 | TOTAL PRESS IN RATIO 11.44 0.986 11.62 0.984 11.66 0.993 11.53 0.998 11.42 0.993 11.21 0.993 10.99 0.999 10.97 0.993 |
|-----------------------|--|--|--|---|---|
| RP - 23456789 | ABS VEL IN OUT 158.5 147.0 167.6 153.8 170.6 156.1 174.3 162.5 173.5 162.6 174.5 160.6 170.9 157.9 162.0 150.7 161.3 146.2 | REL VEL IN OUT 158.3 147.0 167.6 153.8 170.6 156.1 174.3 162.5 173.5 162.6 174.5 160.6 170.9 157.9 162.0 150.7 161.3 146.2 | MERID VEL IN OUT 137.0 146.7 147.6 153.5 150.1 155.8 150.5 162.1 145.4 162.3 143.1 160.5 136.4 157.7 127.0 150.3 124.6 145.5 | TANG VEL IN OUT 79.2 -9.7 79.4 -9.6 81.1 -10.0 88.0 -10.7 94.7 -9.7 99.8 -6.4 102.9 -7.6 100.6 -9.9 102.4 -15.0 | WHEEL SPEED IN OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. |
| RP 1 23 4 5 6 7 8 9 | ABS MACH NO IN OUT 0.464 0.431 0.493 0.451 0.502 0.459 0.515 0.479 0.514 0.480 0.517 0.475 0.507 0.467 0.480 0.445 0.478 0.432 | REL MACH NO IN OUT 0.464 0.431 0.493 0.451 0.502 0.459 0.515 0.479 0.514 0.480 0.517 0.475 0.507 0.467 0.480 0.445 0.478 0.432 | MERID MACH NO IN OUT 0.402 0.430 0.434 0.450 0.442 0.458 0.444 0.478 0.430 0.479 0.424 0.474 0.405 0.466 0.376 0.444 0.369 0.429 | | MERID PEAK SS VEL R MACH NO 1.071 0.464 1.040 0.493 1.038 0.502 1.077 0.515 1.116 0.514 1.121 0.517 1.156 0.507 1.184 0.480 1.167 0.478 |
| RP : 23 4 5 6 7 8 9 | PERCENT INCI SPAN MEAN 5.00 -10.4 10.00 -12.3 15.00 -12.2 30.00 -10.7 50.00 -8.4 70.00 -6.9 85.00 -5.2 90.00 -3.9 95.00 -3.0 | DENCE DEV 11.9 11.7 11.3 10.3 9.6 9.4 8.2 6.9 4.5 | D-FACT EFF 0.454 0. 0.434 0. 0.429 0. 0.403 0. 0.375 0. 0.352 0. 0.330 0. 0.327 0. 0.356 0. | LOSS COEFF TOT PROF 0.105 0.105 0.106 0.106 0.101 0.101 0.039 0.039 0.011 0.011 0.043 0.043 0.041 0.041 0.008 0.008 0.052 0.052 | LOSS PARAM TOT PROF 0.071 0.071 0.070 0.070 0.065 0.065 0.023 0.023 0.006 0.006 0.020 0.020 0.017 0.017 0.003 0.003 0.019 0.019 |

(d) 80 Percent of design speed; reading 1641

| RP 1 2 3 4 5 6 7 8 9 | RAD IN 25.230 2 24.547 2 23.876 2 19.164 1 16.502 1 14.519 1 13.858 1 13.200 1 | 0UT 25.298 24.671 24.049 22.222 19.827 17.465 15.682 | ABS IN 36.0 33.4 33.0 33.5 35.8 37.4 39.2 40.2 41.3 | BETAM OUT -2.2 -2.1 -2.5 -2.7 -2.5 -1.0 -2.7 -5.3 -7.2 | REL IN 36.0 33.4 33.0 33.5 35.8 37.4 39.2 40.2 41.3 | BETAM 0UT -2.2 -2.1 -2.5 -2.7 -2.5 -1.0 -2.7 -5.3 -7.2 | TOTA IN 303.3 302.7 302.6 301.1 299.5 298.1 296.8 296.4 296.5 | RAT10 0.997 0.997 0.997 0.998 0.998 0.998 1.000 1.001 | TOTAL IN 11.51 11.61 11.67 11.70 11.58 11.41 11.16 11.02 | PRESS RATIO 0.987 0.989 0.983 0.995 0.995 0.995 0.995 |
|----------------------|---|--|---|--|---|--|--|---|--|--|
| RP 1 2 3 4 5 6 7 8 9 | ABS IN 149.7 156.3 160.2 166.4 165.9 164.0 157.3 151.9 | VEL 0UT 135.6 142.1 144.8 151.2 149.7 143.6 136.9 130.8 127.9 | REL IN 149.7 156.3 160.2 166.4 165.9 164.0 157.3 151.9 | VEL 0UT 135.6 142.1 144.8 151.2 149.7 143.6 136.9 130.8 127.9 | MERII IN 121.1 130.5 134.4 138.8 134.5 130.2 122.0 116.0 | D VEL OUT 135.5 142.0 144.6 151.0 149.6 143.6 136.7 130.2 126.9 | TAN IN 87.9 86.1 87.2 91.8 97.1 99.7 99.4 98.1 | G VEL OUT -5.2 -6.4 -7.2 -6.5 -2.6 -6.5 -12.2 -15.9 | WHEEL !N 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. | SPEED OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. |
| RP 1 2 3 4 5 6 7 8 9 | ABS MAIN 0.437 0.458 0.470 0.490 0.489 0.485 0.465 0.449 0.449 | ACH NO OUT 0.395 0.415 0.423 0.444 0.440 0.423 0.403 0.384 0.376 | REL M IN 0.437 0.458 0.470 0.490 0.489 0.485 0.465 0.449 | ACH NO OUT 0.395 0.415 0.423 0.444 0.440 0.423 0.403 0.384 0.376 | MERID M IN 0.354 0.382 0.394 0.408 0.397 0.385 0.361 0.343 | ACH NO OUT 0.395 0.415 0.423 0.443 0.440 0.423 0.402 0.383 0.373 | | | | PEAK SS MACH NO 0.437 0.458 0.470 0.490 0.485 0.465 0.449 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INCI MEAN -4.5 -7.1 -7.6 -7.5 -5.6 -4.4 -3.0 -2.1 | DENCE | DEV 13.4 13.2 12.5 11.3 10.5 10.7 8.2 5.3 3.3 | D-FACT 0.518 0.478 0.473 0.443 0.421 0.402 0.395 0.413 0.434 | EFF 0. 0. 0. 0. 0. | LOSS C TOT 0.105 0.084 0.083 0.046 0.034 0.050 0.051 0.038 0.066 | OEFF PROF 0.105 0.084 0.083 0.046 0.034 0.050 0.051 0.038 0.066 | LOSS P TOT 0.072 0.056 0.053 0.027 0.018 0.023 0.021 0.015 0.024 | ARAM PROF 0.072 0.056 0.053 0.027 0.018 0.023 0.021 0.015 |

(e) 80 Percent of design speed; reading 1642

| RP 1 2 3 4 5 6 7 8 9 | RAD IN 25.230 24.547 23.876 21.847 19.164 16.502 14.519 13.858 13.200 | 0UT 25.298 24.671 24.049 22.222 19.827 17.465 15.682 | ABS IN 50.8 45.8 42.9 36.7 38.7 39.3 40.0 40.9 42.0 | BETAM OUT 1.1 1.1 -0.1 -1.1 -1.0 0.1 -2.2 -4.9 -8.6 | IN 50.8 45.8 42.9 36.7 38.7 39.3 40.0 | BETAM OUT 1.1 1.1 -0.1 -1.1 -1.0 0.1 -2.2 -4.9 -8.6 | TOTA IN 305.0 303.9 303.1 301.6 300.0 298.2 296.8 296.6 296.5 | RATIO 0.995 0.996 0.997 0.997 0.997 0.998 1.001 1.002 | TOTAL IN 11.47 11.47 11.67 11.60 11.39 11.17 11.09 | PRESS RATIO 0.990 0.993 0.995 0.988 0.992 0.990 0.990 0.993 |
|---|---|--|--|---|--|---|---|--|--|--|
| R 1 25456789 | ABS IN 140.6 143.7 146.3 159.4 161.2 157.9 153.2 159.3 | VEL 0UT 123.2 126.5 128.7 137.4 138.9 132.4 124.3 121.3 | REL IN 140.6 143.7 146.3 159.4 161.2 157.9 153.2 150.0 149.3 | VEL 0UT 123.2 126.5 128.7 137.4 138.9 132.4 124.3 121.3 117.5 | MERII IN 88.9 100.3 107.2 127.8 125.8 122.2 117.3 113.3 | VEL 0UT 123.2 126.4 128.7 137.4 138.9 132.4 124.2 120.9 116.2 | TAN !N 109.0 103.0 99.6 95.2 100.7 100.0 98.5 98.2 99.9 | G VEL OUT 2.3 2.4 -0.2 -2.7 -2.4 0.2 -4.9 -10.4 -17.6 | WHEEL IN 0. 0. 0. 0. 0. | SPEED OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. |
| R 1 2 5 4 5 6 7 8 9 | ABS MA IN 0.408 0.418 0.427 0.468 0.475 0.466 0.452 0.443 0.441 | OUT 0.357 0.367 0.375 0.402 0.407 0.389 0.364 0.356 0.344 | REL M IN 0.408 0.418 0.427 0.468 0.475 0.466 0.452 0.443 0.441 | 0.357 0.357 0.367 0.375 0.402 0.407 0.389 0.364 0.356 | MERID M IN 0.258 0.292 0.313 0.375 0.371 0.360 0.346 0.335 0.328 | OUT 0.357 0.367 0.375 0.402 0.407 0.389 0.364 0.354 | | | | PEAK SS MACH NG 0.590 0.529 0.489 0.468 0.475 0.466 0.452 0.443 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 :5.00 30.00 50.00 70.00 85.00 90.00 95.00 | !NC! MEAN 10.3 5.2 2.3 -4.3 -2.8 -2.5 -2.2 -1.4 -0.4 | DENCE | DEV 16.7 16.4 14.9 12.9 12.0 11.8 8.7 5.8 1.8 | D-FACT 0.640 0.584 0.560 0.500 0.469 0.443 0.454 0.464 | EFF 0. 0. 0. 0. 0. 0. 0. | LOSS C TOT 0.095 0.062 0.045 0.085 0.057 0.074 0.077 0.057 | 0EFF PROF 0.095 0.062 0.045 0.085 0.057 0.074 0.077 0.057 | LOSS P TOT 0.065 0.041 0.029 0.051 0.030 0.034 0.031 0.022 0.026 | PROF 0.065 0.041 0.029 0.051 0.030 0.034 0.031 0.022 0.026 |

(f) 90 Percent of design speed; reading 1636

| RP 1 2 3 4 5 6 7 8 9 | RAD IN 25.230 2 24.547 2 23.876 2 1.847 2 19.164 1 16.502 1 14.519 1 13.858 1 13.200 1 | 0UT 25.298 24.671 24.049 22.222 19.827 17.465 15.682 | ABS IN 24.4 23.0 23.8 26.2 28.8 30.3 32.7 34.3 35.2 | BETAM OUT -5.5 -5.0 -4.6 -4.0 -3.5 -3.0 -3.6 -5.0 -6.4 | REL IN 24.4 23.0 23.8 26.2 28.8 30.3 32.7 34.3 35.2 | BETAM OUT -5.5 -5.0 -4.6 -4.0 -3.5 -3.0 -3.6 -5.0 -6.4 | TOTA IN 304.9 304.4 304.2 303.7 302.4 300.9 299.5 298.5 297.9 | RATIO 0.991 0.993 0.993 0.994 0.997 0.999 1.002 1.004 | TOTAL IN 11.64 11.90 11.87 11.87 11.50 11.23 10.68 | PRESS RATIO 0.951 0.957 0.971 0.985 0.995 0.996 0.989 0.993 |
|---|--|--|--|---|--|--|--|---|--|---|
| RP 1 23 4 5 6 7 8 9 | ABS IN 206.5 217.5 219.0 225.7 230.1 228.8 222.7 210.7 204.2 | VEL 0UT 195.3 206.4 210.8 220.4 226.1 230.9 231.7 221.2 213.8 | REL IN 206.5 217.5 219.0 225.7 230.1 228.8 222.7 210.7 204.2 | VEL 0UT 195.3 206.4 210.8 220.4 226.1 230.9 231.7 221.2 213.8 | MERII 1N 188.1 200.2 200.5 202.6 201.6 197.5 187.3 174.0 166.8 | D VEL 0UT 194.4 205.6 210.2 219.9 225.7 230.6 231.3 220.3 212.4 | TAN IN 85.2 85.1 88.2 99.6 110.9 115.3 120.5 118.8 117.7 | G VEL OUT -18.9 -18.0 -16.8 -15.4 -13.9 -12.2 -14.6 -19.4 -23.7 | WHEEL IN 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. | SPEED OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. |
| RP 1 2 3 4 5 6 7 8 9 | ABS MA IN 0.612 0.647 0.653 0.675 0.691 0.688 0.670 0.632 0.612 | OUT 0.579 0.614 0.628 0.660 0.679 0.696 0.695 0.665 | REL M IN 0.612 0.647 0.653 0.675 0.691 0.688 0.670 0.632 0.612 | OUT 0.579 0.614 0.628 0.660 0.679 0.696 0.699 0.665 0.641 | MERID M IN 0.557 0.596 0.597 0.606 0.605 0.594 0.564 0.522 0.500 | ACH NO OUT 0.576 0.612 0.626 0.658 0.678 0.695 0.698 0.662 0.637 | | | | PEAK SS MACH NO 0.612 0.647 0.653 0.675 0.691 0.688 0.670 0.632 0.612 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INC II MEAN -16.1 -17.5 -16.9 -14.8 -12.6 -11.5 -9.5 -8.0 -7.2 | DENCE | DEV 10.1 10.3 10.4 10.0 9.5 8.7 7.3 5.7 | D-FACT 0.398 0.365 0.347 0.324 0.299 0.240 0.199 0.198 0.203 | EFF 0. 0. 0. 0. 0. 0. 0. | LOSS C TOT 0.222 0.173 0.115 0.059 0.020 0.015 0.042 0.032 0.039 | OEFF PROF 0.222 0.173 0.115 0.059 0.020 0.015 0.042 0.032 0.039 | LOSS P TOT 0.151 0.115 0.074 0.035 0.010 0.007 0.017 0.012 0.014 | PROF 0.151 0.115 0.074 0.035 0.010 0.007 0.017 0.012 0.014 |

(g) 90 Percent of design speed; reading 1637

| RP 1 2 3 4 5 6 7 8 9 | RADI IN 25.230 2 24.547 2 23.876 2 21.847 2 19.164 1 16.502 1 14.519 1 13.858 1 13.200 1 | 0UT 5.298 4.671 4.049 2.222 9.827 7.465 5.682 5.070 | ABS IN 26.6 25.6 25.4 27.9 30.6 32.9 35.1 36.7 37.7 | BETAM OUT -4.8 -4.5 -4.3 -3.9 -2.8 -3.1 -4.1 -5.6 | REL IN 26.6 25.6 25.4 27.9 30.6 32.9 35.1 36.7 37.7 | BETAM OUT -4.8 -4.5 -4.3 -3.9 -2.8 -3.1 -4.1 -5.6 | TOTAL IN 304.9 304.4 304.3 303.3 302.0 300.9 299.8 298.8 298.8 | TEMP RATIO 0.994 0.994 0.997 0.998 0.999 1.001 1.003 | TOTAL IN 11.82 12.00 12.07 12.02 11.87 11.74 11.52 11.19 | PRESS RATIO 0.967 0.973 0.977 0.992 0.998 0.993 0.989 1.000 0.992 |
|---|--|---|--|---|--|---|--|--|---|---|
| RP 1 2 3 4 5 6 7 8 9 | 199.4 203.3 207.2 207.7 209.7 207.4 196.1 | VEL 0UT 174.8 184.4 188.2 196.2 198.9 201.3 201.6 194.8 188.5 | REL IN 190.7 199.4 203.3 207.2 207.7 209.7 207.4 196.1 192.9 | VEL 0UT 174.8 184.4 188.2 196.2 198.9 201.3 201.6 194.8 188.5 | MERII 1N 170.5 179.8 183.6 183.0 178.7 176.1 169.6 157.2 152.5 | VEL 0UT 174.2 183.8 187.6 195.6 198.5 201.1 201.3 194.3 187.6 | TAN IN 85.2 86.1 87.3 97.1 105.8 113.8 119.3 117.1 | G VEL OUT -14.5 -14.6 -14.1 -14.7 -13.4 -9.8 -10.9 -14.0 -18.3 | WHEEL IN 0. 0. 0. 0. 0. | SPEED OUT 0. 0. 0. 0. 0. |
| RP 1 2 3 4 5 6 7 8 9 | 0.589 0.602 0.616 0.619 0.626 0.620 0.585 | OUT 0.514 0.544 0.556 0.582 0.591 0.600 0.601 0.580 0.560 | REL M. 1N 0.562 0.589 0.602 0.616 0.619 0.626 0.620 0.585 0.575 | OUT 0.514 0.556 0.556 0.591 0.600 0.580 0.560 | MERID M IN 0.502 0.532 0.544 0.544 0.532 0.526 0.507 0.469 0.455 | OUT 0.512 0.542 0.555 0.580 0.590 0.599 0.600 0.578 0.557 | | | | PEAK SS MACH NO 0.562 0.589 0.602 0.616 0.619 0.626 0.620 0.585 0.575 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INCI MEAN -13.9 -15.0 -15.2 -13.1 -10.8 -8.9 -7.1 -5.6 -4.7 | DENCE | DEV 10.9 10.8 10.7 9.7 9.2 9.0 7.9 6.6 4.8 | D-FACT 0.439 0.410 0.396 0.372 0.340 0.304 0.275 0.259 0.278 | EFF 0. 0. 0. 0. 0. | LOSS C TOT 0.169 0.128 0.105 0.035 0.011 0.029 0.048 0.001 | OEFF PROF 0.169 0.128 0.105 0.035 0.011 0.029 0.048 0.001 | LOSS F TOT 0.115 0.085 0.068 0.021 0.006 0.013 0.019 0.000 | PROF 0.115 0.085 0.068 0.021 0.006 0.013 0.019 0.000 |

(h) 90 Percent of design speed; reading 1632

| RP 1 2 3 4 5 6 7 8 9 | RADII IN OU 25.230 25.2 24.547 24.6 23.876 24.0 21.847 22.2 19.164 19.8 16.502 17.4 14.519 15.6 13.858 15.0 13.200 14.4 | T IN 98 30.8 71 28.7 49 28.1 22 30.4 27 33.7 65 35.5 82 37.6 70 39.2 | BETAM OUT -3.8 -2.1 -3.7 -3.6 -2.8 -1.8 -2.2 -3.5 -5.9 | REL IN 30.8 28.7 28.1 30.4 33.7 35.5 37.6 39.2 40.3 | BETAM OUT -3.8 -2.1 -3.7 -3.6 -2.8 -1.8 -2.2 -3.5 -5.9 | IN 306.0 305.8 305.5 304.2 302.8 301.1 299.8 | TEMP RATIO 0.997 0.998 0.997 0.998 0.999 1.000 1.001 0.999 | TOTAL IN 11.83 12.06 12.12 12.13 11.99 11.77 11.52 11.26 | PRESS RATIO 0.980 0.977 0.980 0.990 0.994 0.992 0.992 0.997 0.987 |
|----------------------|---|---|--|--|---|--|---|---|---|
| R 1 2 5 4 15 6 1 8 9 | ABS VEL IN 00' 178.4 164 188.2 171 192.7 174 197.7 181 197.2 182 196.1 179 191.4 175 182.8 167 182.1 161 | T IN 178.4 .0 188.2 .9 192.7 .7 197.7 .0 197.2 .3 196.1 .6 191.4 .5 182.8 | VEL 0UT 164.2 171.0 174.9 181.7 182.0 179.3 175.6 167.5 161.6 | MERII IN 153.2 165.1 169.9 170.5 164.0 159.6 151.7 141.7 139.0 | VEL 0UT 163.8 170.9 174.5 181.3 181.8 179.2 175.5 167.2 160.7 | IN 91.3 90.4 90.9 100.1 109.4 | | WHEEL IN 0. 0. 0. 0. | SPEED OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. |
| RP 1 2 3 4 5 6 7 8 9 | ABS MACH IN OU 0.522 0.4 0.553 0.5 0.567 0.5 0.584 0.5 0.583 0.5 0.569 0.5 0.542 0.4 0.540 0.4 | T IN 79 0.522 01 0.553 13 0.567 35 0.584 37 0.584 30 0.583 19 0.569 95 0.542 | ACH NO OUT 0.479 0.501 0.513 0.535 0.537 0.530 0.519 0.495 0.477 | 0.500 0.504 0.486 | 0.478 0.478 0.500 0.512 0.534 0.536 0.530 0.519 0.474 | | | | |
| RP 1 2 3 4 5 6 7 8 9 | SPAN M 5.00 -1 10.00 -1 15.00 -1 30.00 -1 50.00 - 70.00 - 85.00 - 90.00 - | INCIDENCE EAN 9.7 1.8 2.5 0.6 7.7 6.3 4.6 3.1 2.1 | DEV 11.8 13.2 11.3 10.5 10.2 10.0 8.7 7.2 4.5 | D-FACT 0.471 0.431 0.434 0.414 0.388 0.358 0.337 0.342 0.378 | EFF 0. 0. 0. 0. 0. 0. 0. | LOSS C TOT 0.120 0.123 0.100 0.050 0.031 0.037 0.040 0.019 0.072 | OEFF PROF 0.120 0.123 0.100 0.050 0.031 0.037 0.040 0.019 0.072 | LOSS F TOT 0.082 0.082 0.064 0.030 0.016 0.017 0.016 0.007 | PROF 0.082 0.082 0.064 0.030 0.016 0.017 0.016 |

(i) 90 Percent of design speed; reading 1633

| RP 1 2 3 4 5 6 7 8 9 | RADI IN 25.230 25 24.547 25 23.876 25 21.847 25 19.164 15 16.502 15 14.519 15 13.858 15 13.200 14 | 0UT 5.298 4.671 4.049 2.222 9.827 7.465 5.682 5.070 | ABS 1N 35.6 33.3 32.2 32.9 36.1 37.6 39.4 40.6 41.8 | BETAM OUT -2.4 -2.3 -2.5 -2.8 -2.2 -0.9 -2.3 -4.3 -6.8 | REL 1N 35.6 33.3 32.2 32.9 36.1 37.6 39.4 40.6 41.8 | BETAM OUT -2.4 -2.3 -2.5 -2.8 -2.2 -0.9 -2.3 -4.3 -6.8 | TOTA IN 306.9 306.2 305.9 304.5 302.9 301.1 299.4 299.0 298.9 | L TEMP RATIO 0.997 0.998 0.998 0.998 0.999 1.002 1.001 | TOTAL IN 11.83 11.99 12.09 12.13 11.99 11.78 11.45 11.32 | PRESS RATIO 0.986 0.984 0.992 0.994 0.990 0.991 0.992 0.985 |
|---|---|---|--|---|--|--|--|---|---|---|
| RP 1 23 4 5 6 7 8 9 | 175.9 181.6 188.2 187.7 186.4 178.3 | VEL 0UT 151.9 158.9 162.7 170.4 169.9 163.7 154.6 149.2 144.8 | REL IN 167.9 175.9 181.6 188.2 187.7 186.4 178.3 173.6 173.5 | VEL 0UT 151.9 158.9 162.7 170.4 169.9 163.7 154.6 149.2 144.8 | MERII IN 136.5 147.0 153.6 158.0 151.8 147.7 137.9 131.7 129.3 | VEL OUT 151.8 158.8 162.5 170.2 169.8 163.7 154.5 148.8 143.8 | TAN !N 97.6 96.7 96.8 102.3 110.5 113.7 113.1 113.0 115.7 | G VEL OUT -6.5 -6.2 -7.2 -8.3 -6.4 -2.5 -6.2 -11.1 -17.2 | WHEEL IN 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. | SPEED OUT 0. 0. 0. 0. |
| RP ! 23 4 5 6 7 8 9 | 0.515 0.532 0.554 0.554 0.552 0.528 0.514 | CH NO OUT 0.442 0.463 0.475 0.500 0.499 0.482 0.454 0.438 0.425 | REL M. 1N 0.489 0.515 0.532 0.554 0.552 0.552 0.514 0.514 | 0.442 0.463 0.475 0.500 0.499 0.482 0.454 0.438 | MERID M. iN 0.398 0.430 0.450 0.465 0.448 0.437 0.408 0.390 0.383 | ACH NO OUT 0.441 0.463 0.474 0.499 0.499 0.482 0.454 0.437 0.422 | | | | PEAK SS MACH NO 0.489 0.515 0.532 0.554 0.552 0.528 0.514 |
| RP ! 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INCII MEAN -4.9 -7.2 -8.4 -8.1 -5.4 -4.3 -2.9 -1.7 -0.6 | DENCE | DEV 13.2 13.1 12.4 11.2 10.9 10.9 8.6 6.4 3.6 | D-FACT 0.518 0.485 0.474 0.441 0.417 0.399 0.396 0.409 0.442 | EFF 0. 0. 0. 0. 0. 0. | LOSS C TOT 0.095 0.095 0.091 0.044 0.031 0.054 0.051 0.050 0.090 | OEFF PROF 0.095 0.095 0.091 0.044 0.031 0.054 0.051 0.050 0.090 | LOSS P TOT 0.065 0.063 0.059 0.026 0.016 0.025 0.021 0.019 | ARAM PROF 0.065 0.063 0.059 0.026 0.016 0.025 0.021 0.019 0.033 |

TABLE VIII. - Continued.

(j) 90 Percent of design speed; reading 1634

| RP 1 2 3 4 5 6 7 8 9 | RADI IN 25.230 2 24.547 2 23.876 2 21.847 2 19.164 1 16.502 1 14.519 1 13.858 1 13.200 1 | 0UT 25.298 24.671 24.049 22.222 9.827 7.465 5.682 | ABS IN 44.9 40.4 38.0 35.7 37.9 38.9 40.4 41.3 42.4 | BETAM OUT -0.3 -0.3 -1.0 -1.3 -1.3 0.0 -2.4 -4.8 -6.9 | IN 44.9 40.4 38.0 35.7 37.9 38.9 40.4 41.3 | BETAM OUT -0.3 -0.3 -1.0 -1.3 -1.3 0.0 -2.4 -4.8 -6.9 | | IN RATIO 11.84 0.987 11.90 0.989 11.97 0.989 12.13 0.990 12.02 0.991 11.75 0.987 11.45 0.989 |
|----------------------|--|---|---|---|---|---|---|---|
| RP 1 23456789 | 170.8 181.7 183.1 179.6 173.5 169.4 | VEL 0UT 141.4 146.6 150.1 160.1 159.5 151.3 142.1 137.5 135.3 | | VEL 0UT 141:4 146.6 150.1 160.1 159.5 151.3 142.1 137.5 135.3 | IN 113.7 125.8 134.7 147.6 144.5 139.8 132.2 | VEL OUT 141.4 146.6 150.1 160.0 159.4 151.3 142.0 137.0 134.3 | TANG VEL IN OUT 113.2 -0.7 107.2 -0.8 105.1 -2.6 105.9 -3.7 112.3 -3.7 112.8 0.1 112.4 -5.9 111.8 -11.6 114.3 -16.3 | 0. 0. 0. 0. 0. 0. 0. 0. |
| RP 1 2 3 4 5 6 7 8 9 | 0.498 0.533 0.539 0.531 0.513 | CH NO CUT 0.409 0.425 0.436 0.467 0.467 0.444 0.417 0.403 0.394 | IN 0.466 0.481 0.498 0.533 0.539 | OUT 0.409 0.425 0.436 0.467 0.467 0.444 0.417 0.403 0.394 | 0.393 0.433 0.426 | OUT 0.409 0.425 0.436 0.467 0.467 0.444 0.416 0.401 | | MERID PEAK SS VEL R MACH NG 1.243 0.574 1.166 0.481 1.115 0.498 1.084 0.533 1.103 0.539 1.082 0.531 1.074 0.513 1.077 0.501 1.074 0.505 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INC II MEAN 4.4 -0.1 -2.6 -5.3 -3.6 -2.9 -1.8 -1.0 | DENCE | DEV 15.4 15.0 14.0 12.7 11.7 11.8 8.6 5.8 3.5 | D-FACT 0.603 0.546 0.528 0.475 0.457 0.437 0.449 0.463 0.479 | EFF 0. 0. 0. 0. 0. | LOSS COEFF TOT PROF 0.096 0.096 0.074 0.074 0.069 0.069 0.059 0.059 0.049 0.049 0.076 0.076 0.076 0.076 0.068 0.068 0.092 0.092 | LOSS PARAM TOT PROF 0.065 0.065 0.049 0.049 0.045 0.045 0.035 0.035 0.026 0.026 0.035 0.031 0.026 0.026 0.034 0.034 |

(k) 100 Percent of design speed; reading 1625

| RP 1 2 3 4 5 6 7 8 9 | RADII IN 25.230 25 24.547 24 23.876 24 21.847 22 19.164 19 16.502 17 14.519 15 13.858 15 13.200 14 | 0UT .298 .671 .049 .222 .827 .465 .682 .070 | ABS IN 28.4 25.9 26.3 28.5 31.0 33.2 36.2 37.5 38.2 | BETAM OUT -5.3 -4.8 -4.5 -4.3 -3.7 -2.5 -2.9 -4.2 -6.1 | REL IN 28.4 25.9 26.3 28.5 31.0 33.2 36.2 37.5 38.2 | BETAM OUT -5.3 -4.8 -4.5 -4.3 -3.7 -2.5 -2.9 -4.2 -6.1 | TOTA IN 309.6 309.1 309.0 307.8 305.9 304.5 302.5 301.5 | RAT10 0.997 0.997 0.997 0.999 1.002 1.001 1.002 1.003 | TOTAL IN 12.03 12.44 12.49 12.53 12.34 12.16 11.79 11.43 | PRESS RAT10 0.967 0.960 0.969 0.984 0.998 0.990 0.991 1.003 0.990 |
|---|--|--|--|---|--|--|---|--|---|---|
| RP 1 234 5 67 8 9 | 208.1 1 223.4 2 226.9 2 234.6 2 234.9 2 234.4 2 225.7 2 214.7 2 | OUT 92.5 03.8 08.7 20.1 | REL IN 208.1 223.4 226.9 234.6 234.9 234.4 225.7 214.7 212.6 | VEL 0UT 192.5 203.8 208.7 220.1 225.1 223.8 219.7 212.3 205.0 | MERII IN 183.0 201.0 203.4 206.2 201.3 196.0 182.1 170.2 167.1 | VEL 0UT 191.7 203.1 208.1 219.5 224.6 223.6 219.4 211.7 203.8 | TAN IN 99.1 97.6 100.6 111.9 121.0 128.5 133.4 130.8 | G VEL OUT -17.9 -16.9 -16.4 -16.3 -14.5 -9.7 -11.0 -15.6 -21.9 | WHEEL IN 0. 0. 0. 0. 0. | SPEED OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. |
| RP 1 2 3 4 5 6 7 8 9 | 0.612 0 0.661 0 0.672 0 0.699 0 0.702 0 0.702 0 0.676 0 0.642 0 | H NO 0UT .564 .599 .615 .652 .669 .656 .656 | REL M IN 0.612 0.661 0.672 0.699 0.702 0.702 0.676 0.642 0.635 | ACH NO 0UT 0.564 0.599 0.615 0.6652 0.6667 0.656 0.656 | MERID M 1N 0.538 0.595 0.603 0.614 0.602 0.587 0.546 0.509 0.499 | ACH NO OUT 0.561 0.597 0.613 0.650 0.668 0.667 0.655 0.631 0.607 | | | | PEAK SS MACH NO 0.612 0.661 0.672 0.699 0.702 0.702 0.676 0.642 0.635 |
| RP 1 2 3 4 5 6 7 8 9 | 10.00 15.00 30.00 | INCID MEAN -12.0 -14.6 -14.3 -12.5 -10.4 -8.6 -6.0 -4.8 -4.2 | DENCE | DEV 10.5 10.5 9.3 9.3 9.1 6.5 4.3 | D-FACT 0.458 0.428 0.413 0.384 0.341 0.309 0.279 0.268 0.296 | EFF 0. 0. 0. 0. 0. | LOSS C TOT 0.148 0.158 0.119 0.057 0.009 0.035 0.033 -0.011 0.041 | PROF 0.148 0.158 0.119 0.057 0.009 0.035 0.033 | LOSS F TOT 0.101 0.105 0.077 0.034 0.005 0.016 0.013 -0.004 0.015 | PROF 0.101 0.105 0.077 0.034 0.005 0.016 0.013 |

TABLE VIII. - Continued.

(1) 100 Percent of design speed; reading 1626

| RP 1 23 4 5 6 7 8 9 | RADI IN 25.230 2 24.547 2 23.876 2 21.847 2 19.164 1 16.502 1 14.519 1 13.858 1 13.200 1 | 0UT 25.298 24.671 24.049 22.222 19.827 17.465 15.682 | ABS IN 30.7 28.4 28.5 30.5 33.5 35.3 37.6 39.1 39.8 | BETAM 0UT -4.3 -4.0 -3.9 -3.7 -3.1 -1.7 -2.5 -3.9 -6.5 | REL IN 30.7 28.4 28.5 30.5 33.5 35.3 37.6 39.1 | BETAM OUT -4.3 -4.0 -3.9 -3.7 -3.1 -1.7 -2.5 -3.9 -6.5 | TOTA IN 310.1 309.9 309.7 308.0 306.1 304.2 302.7 301.8 301.7 | RATIO 0.997 0.996 0.996 0.999 1.000 1.001 1.002 1.002 | TOTAL IN 12.30 12.55 12.63 12.65 12.41 12.21 11.82 11.52 | PRESS RATIO 0.973 0.971 0.974 0.987 0.995 0.988 0.994 0.997 0.987 |
|---|--|---|---|---|--|--|--|---|---|---|
| R 1 23 4 5 67 8 9 | 221.8 223.0 215.7 | VEL 0UT 183.6 191.7 195.4 205.3 206.3 204.7 202.0 192.8 186.2 | IN 200.9 211.4 216.1 222.6 221.8 223.0 215.7 | VEL 0UT 183.6 191.7 195.4 205.3 206.3 204.7 202.0 192.8 186.2 | MERII 1N 172.7 185.9 189.9 191.8 185.0 182.0 170.9 160.1 157.3 | VEL OUT 183.1 191.2 194.9 204.9 204.6 201.8 192.4 185.0 | IN 102.7 100.6 103.1 113.1 122.4 128.8 | G VEL OUT -13.7 -13.4 -13.3 -13.4 -11.3 -6.1 -8.7 -13.1 -21.1 | WHEEL IN 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. | SPEED OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. |
| RP 1 2 3 4 5 6 7 8 9 | ABS MAIN 0.588 0.622 0.637 0.660 0.659 0.643 0.614 0.609 | OUT 0.535 0.561 0.573 0.605 0.606 0.599 0.571 0.551 | REL M. IN 0.588 0.622 0.637 0.660 0.659 0.665 0.643 0.614 0.609 | OUT 0.535 0.561 0.573 0.605 0.610 0.606 0.599 0.571 | MERID M IN 0.506 0.547 0.560 0.568 0.550 0.543 0.510 0.477 0.468 | OUT 0.534 0.560 0.572 0.604 0.609 0.606 0.599 0.570 0.547 | | | | PEAK SS MACH NO 0.588 0.622 0.637 0.660 0.659 0.665 0.643 0.614 0.609 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INCII MEAN -9.7 -12.1 -12.1 -10.5 -7.9 -6.5 -4.6 -3.2 -2.6 | DENCE | DEV 11.4 11.3 11.1 10.3 9.9 10.0 8.5 6.8 3.9 | D-FACT 0.481 0.451 0.444 0.413 0.382 0.352 0.319 0.327 0.358 | EFF 0. 0. 0. 0. 0. | LOSS C TOT 0.131 0.127 0.108 0.052 0.019 0.045 0.026 0.013 0.057 | OEFF PROF 0.131 0.127 0.108 0.052 0.019 0.045 0.026 0.013 0.057 | LOSS P TOT 0.089 0.084 0.070 0.031 0.010 0.021 0.011 0.005 | PROF 0.089 0.084 0.070 0.031 0.010 0.021 0.005 0.021 |

(m) 100 Percent design speed; reading 1627

| RP 1 2 3 4 5 6 7 8 9 | RAD IN 25.230 24.547 23.876 21.847 19.164 16.502 14.519 13.858 13.200 | 0UT 25.298 24.671 24.049 22.222 19.827 17.465 15.682 | ABS IN 34.5 32.0 31.2 32.6 35.5 36.8 39.1 40.3 41.0 | BETAM OUT -3.2 -3.1 -3.3 -3.1 -2.6 -1.1 -2.5 -4.1 -6.8 | REL IN 34.5 32.0 31.2 32.6 35.5 36.8 39.1 40.3 41.0 | BETAM 0UT -3.2 -3.1 -3.3 -3.1 -2.6 -1.1 -2.5 -4.1 -6.8 | TOTAL IN 311.1 310.2 310.0 308.5 306.5 304.5 302.7 302.1 302.0 | TEMP RATIO 0.997 0.997 0.999 0.999 0.999 1.001 1.003 | TOTAL IN 12.31 12.49 12.61 12.70 12.45 12.23 11.79 11.57 | PRESS RATIO 0.980 0.979 0.979 0.986 0.995 0.987 0.992 0.997 |
|----------------------|---|--|--|--|--|---|--|--|---|--|
| R : 234567.89 | ABS IN 190.0 198.6 205.0 213.4 212.6 213.8 205.7 198.9 198.7 | VEL 0UT 172.2 178.7 183.4 192.5 193.7 184.2 178.4 171.0 | REL IN 190.0 198.6 205.0 213.4 212.6 213.8 205.7 198.9 198.7 | VEL 0UT 172.2 178.7 183.4 192.5 193.7 184.2 178.4 171.0 | MERII IN 156.5 168.4 175.4 179.8 173.1 171.1 159.7 151.8 150.0 | VEL 0UT 171.9 178.5 183.1 192.2 193.5 189.7 184.1 177.9 169.8 | TAN IN 107.7 105.4 106.2 114.9 123.4 128.2 129.6 128.6 130.4 | G VEL OUT -9.5 -9.7 -10.4 -10.4 -8.7 -3.5 -8.0 -12.7 -20.2 | WHEEL IN 0. 0. 0. 0. 0. | SPEED OUT 0. 0. 0. 0. 0. |
| RP 1 2 3 4 5 6 7 8 9 | ABS MAIN 0.554 0.581 0.602 0.630 0.629 0.635 0.611 0.591 0.590 | OUT 0.500 0.521 0.535 0.564 0.570 0.559 0.543 0.525 0.503 | REL M. 0.554 0.581 0.602 0.630 0.629 0.635 0.611 0.591 0.590 | OUT 0.500 0.521 0.535 0.564 0.570 0.559 0.543 0.525 0.503 | MERID M IN 0.456 0.493 0.515 0.530 0.512 0.508 0.475 0.451 | ACH NO 0.499 0.534 0.5669 0.5559 0.5524 0.500 | | | | PEAK SS MACH NO 0.554 0.581 0.602 0.630 0.629 0.635 0.611 0.591 |
| RP: 23456789 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INC I MEAN -5.9 -8.5 -9.4 -6.0 -5.0 -3.2 -2.0 | DENCE | DEV 12.5 12.2 11.7 10.9 10.5 10.7 8.5 6.6 3.6 | D-FACT 0.514 0.484 0.472 0.444 0.411 0.387 0.367 0.371 0.413 | EFF 0. 0. 0. 0. 0. 0. | LOSS COTOT C.107 0.105 0.095 0.061 0.021 0.056 0.036 0.016 0.082 | DEFF PROF 0.107 0.105 0.095 0.061 0.021 0.056 0.036 0.016 | LOSS P TOT 0.073 0.069 0.061 0.036 0.011 0.026 0.015 0.006 | PROF 0.073 0.069 0.061 0.036 0.011 0.026 0.015 0.006 0.030 |

TABLE VIII. - Continued.

(n) 100 Percent of design speed, reading 1628

| RP 1 2 3 4 5 6 7 8 9 | RAD IN 25.230 2 4.547 2 3.876 2 1.847 1 19.164 1 16.502 1 14.519 1 13.858 1 13.200 | 0UT 25.298 24.671 24.049 22.222 19.827 17.465 15.682 | ABS IN 39.5 35.1 34.7 34.1 37.0 37.8 39.9 40.8 41.7 | BETAM 0UT -1.6 -1.8 -2.5 -2.4 -2.0 -0.6 -2.4 -4.2 -7.2 | REL IN 39.5 35.1 34.7 34.1 37.0 37.8 39.9 40.8 41.7 | BETAM 0UT -1.6 -1.8 -2.5 -2.4 -2.0 -0.6 -2.4 -4.2 -7.2 | TOTA IN 311.6 310.8 310.3 308.9 306.5 304.4 302.5 301.7 301.9 | RATIO 0.998 0.998 0.997 0.998 0.998 0.999 1.001 1.002 | TOTAL IN 12.29 12.45 12.54 12.67 12.44 12.23 11.80 11.59 11.63 | PRESS RATIO 0.983 0.981 0.981 0.987 0.995 0.985 0.988 0.993 0.981 |
|----------------------|--|--|---|---|--|---|--|---|--|---|
| RP 1 23 4 5 6 7 8 9 | ABS IN 182.3 190.8 196.4 205.4 207.0 199.0 192.7 193.6 | VEL 0UT 163.3 169.3 173.1 183.6 183.5 179.0 170.8 164.8 159.5 | REL IN 182.3 190.8 196.4 206.1 205.4 207.0 199.0 192.7 193.6 | VEL 0UT 163.3 169.3 173.1 183.6 183.5 179.0 170.8 164.8 159.5 | MERII 1N 140.7 156.1 161.5 170.7 164.0 163.5 152.6 146.0 144.5 | VEL 0UT 163.2 169.2 172.9 183.4 183.4 179.0 170.6 164.3 158.2 | TAN IN 115.9 109.8 111.8 115.4 123.7 127.0 127.7 125.8 128.9 | G VEL OUT -4.6 -5.3 -7.7 -7.7 -6.5 -1.9 -7.3 -12.1 -20.1 | WHEEL IN 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. | SPEED OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. |
| RP 1 2 3 4 5 6 7 8 9 | ABS MAIN 0.530 0.557 0.574 0.606 0.607 0.614 0.590 0.571 0.574 | OUT 0.472 0.491 0.503 0.536 0.538 0.526 0.502 0.484 0.468 | REL M/ IN 0.530 0.557 0.574 0.606 0.607 0.614 0.590 0.571 0.574 | OUT 0.472 0.491 0.503 0.536 0.538 0.526 0.502 0.484 0.468 | MERID M IN 0.409 0.455 0.472 0.502 0.484 0.485 0.453 0.428 | OUT 0.472 0.491 0.503 0.536 0.538 0.526 0.501 0.482 0.464 | | | | PEAK SS MACH NG 0.530 0.557 0.574 0.606 0.607 0.614 0.590 0.571 0.574 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INCII MEAN -1.0 -5.4 -5.9 -6.9 -4.4 -4.0 -2.3 -1.5 | DENCE | DEV 14.0 13.5 12.4 11.6 11.0 11.1 8.5 6.5 3.2 | D-FACT 0.555 0.513 0.511 0.462 0.435 0.413 0.409 0.414 0.454 | EFF 0. 0. 0. 0. 0. 0. 0. | LOSS C TOT 0.098 0.100 0.095 0.058 0.024 0.068 0.057 0.036 0.095 | OEFF PROF 0.098 0.100 0.095 0.058 0.024 0.068 0.057 0.036 0.095 | LOSS F TOT 0.067 0.061 0.034 0.013 0.031 0.023 0.014 0.035 | PARAM PROF 0.067 0.067 0.061 0.034 0.013 0.031 0.023 0.014 0.035 |

TABLE VIII. - Concluded.

(o) 100 Percent of design speed; reading 1629

| RP 1 2 3 4 5 6 7 8 9 | RADII IN 25.230 25 24.547 24 23.876 24 21.847 22 19.164 19 16.502 17 14.519 15 13.858 15 13.200 14 | .671 .049 .222 .827 .465 .682 | ABS IN 48.2 42.3 39.5 35.9 38.0 38.7 40.0 41.3 42.0 | BETAM OUT -0.6 -0.2 -1.1 -1.3 -1.3 -0.3 -2.5 -5.0 -8.4 | REL IN 48.2 42.3 39.5 35.9 38.0 38.7 40.0 41.3 42.0 | BETAM OUT -0.6 -0.2 -1.1 -1.3 -0.3 -2.5 -5.0 -8.4 | IN 313.6 312.0 311.4 309.3 307.0 304.5 | TEMP RATIO 0.994 0.996 0.996 0.997 0.997 1.001 1.001 | TOTAL IN 12.11 12.24 12.30 12.62 12.46 12.22 11.82 11.64 11.65 | PRESS RATIO 0.989 0.987 0.989 0.983 0.990 0.979 0.981 0.987 |
|---|--|---|---|--|---|---|--|---|--|---|
| RP 1 23 4 5 67: 8 9 | 175.2 19 183.1 19 187.9 10 203.4 10 204.7 10 204.2 10 196.9 10 191.2 10 | 0UT 53.5 58.6 62.7 75.7 77.7 70.4 61.5 56.3 | 191.2 | VEL 0UT 153.5 158.6 162.7 175.7 177.7 170.4 161.5 156.3 151.5 | MERII IN 116.9 135.4 145.0 164.6 161.3 159.4 150.8 143.6 142.3 | VEL 0UT 153.5 158.6 162.6 175.6 177.6 170.4 161.3 155.7 149.9 | TANG IN 130.5 123.3 119.5 119.4 126.1 127.6 126.6 126.3 128.0 | VEL OUT -1.5 -0.7 -3.2 -4.1 -4.2 -0.8 -7.0 -13.5 -22.1 | WHEEL IN 0. 0. 0. 0. 0. | SPEED OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. |
| RP 1 2 3 4 5 6 7 8 9 | 0.506 0 0.532 0 0.547 0 0.597 0 0.604 0 0.605 0 0.584 0 | 0UT .442 .458 .471 .512 .520 .500 .473 | REL MA IN 0.506 0.532 0.547 0.597 0.604 0.605 0.584 0.566 0.567 | OLATA 0.442 0.458 0.471 0.512 0.520 0.520 0.473 0.458 0.443 | MERID MA IN 0.338 0.393 0.422 0.483 0.476 0.472 0.447 0.425 0.421 | OUT 0.442 0.458 0.471 0.512 0.520 0.500 0.473 0.456 0.439 | | | | PEAK SS MACH NO 0.685 0.596 0.547 0.597 0.604 0.605 0.566 0.567 |
| RP 1 2 3 4 5 6 7 8 9 | PERCENT SPAN 5.00 10.00 15.00 30.00 50.00 70.00 85.00 90.00 95.00 | INCID MEAN 7.7 1.8 -1.1 -5.1 -3.4 -3.2 -2.2 -1.0 -0.4 | ENCE | DEV 15,1 15.1 13.8 12.7 11.7 11.5 8.5 5.7 2.0 | D-FACT 0.637 0.582 0.555 0.494 0.461 0.445 0.447 0.458 0.492 | EFF 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. | LOSS C TOT 0.069 0.076 0.062 0.079 0.047 0.097 0.090 0.066 0.103 | 0EFF PROF 0.069 0.076 0.062 0.079 0.047 0.097 0.090 0.066 0.103 | LOSS P TOT 0.047 0.051 0.040 0.047 0.025 0.045 0.037 0.026 0.038 | ARAM PROF 0.047 0.051 0.040 0.047 0.025 0.045 0.037 0.026 0.038 |

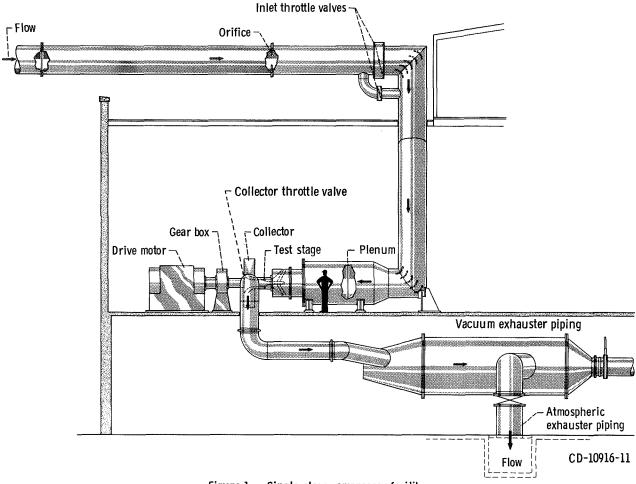


Figure 1. - Single-stage compressor facility.

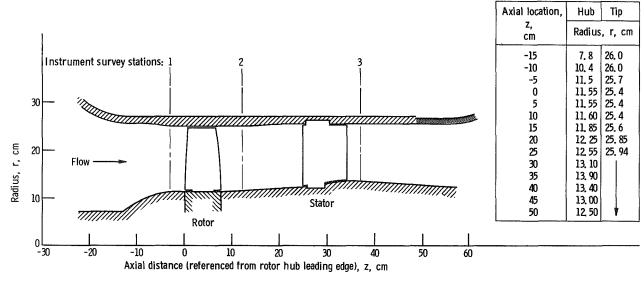
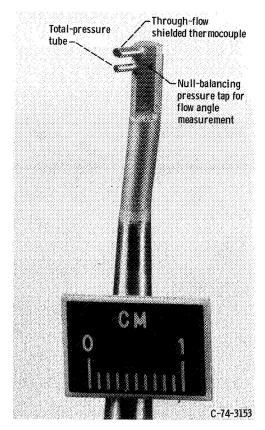
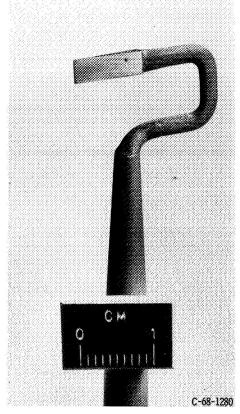


Figure 2. - Fan stage 55 flow path.





(a) Combination total pressure, total temperature, and flow angle probe.

(b) Static-pressure probe; 80 C-shaped wedge.

Figure 3. - Survey probes.

- o Wall static pressure
- ☐ C-shaped static probe
- △ Combination total pressure, total temperature, and angle probe

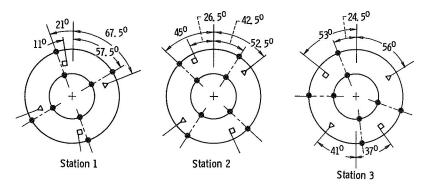
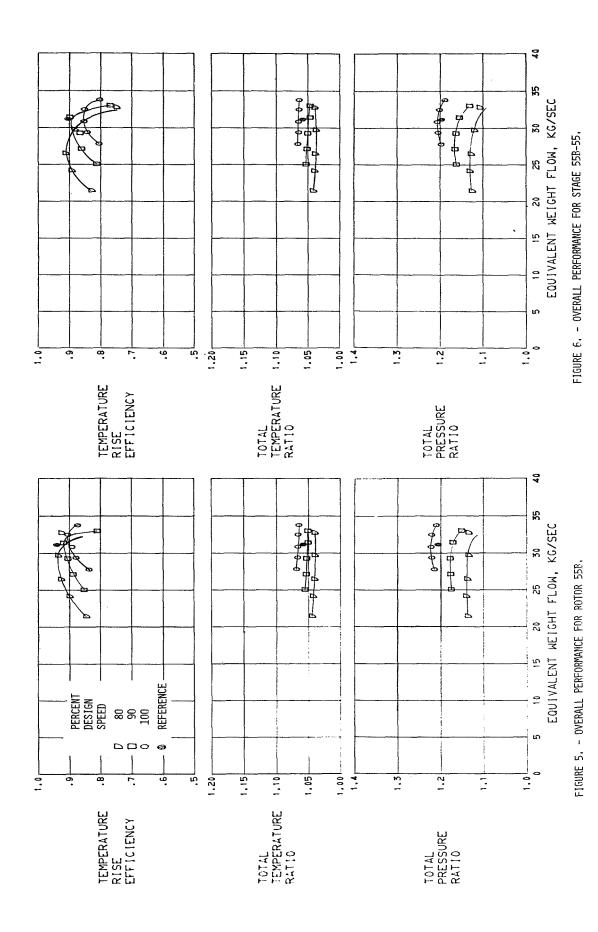
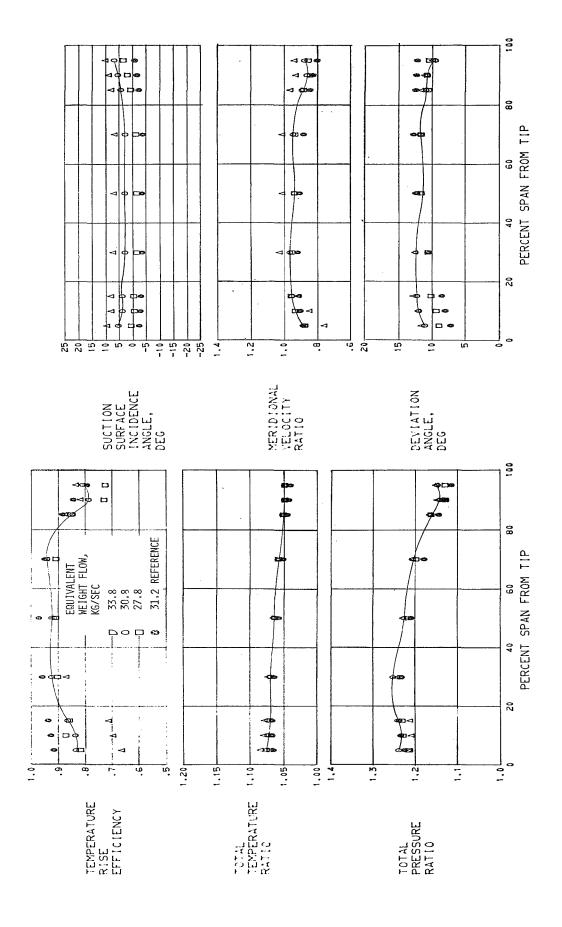


Figure 4. - Circumferential location of survey instrumentation at each station looking downstream.





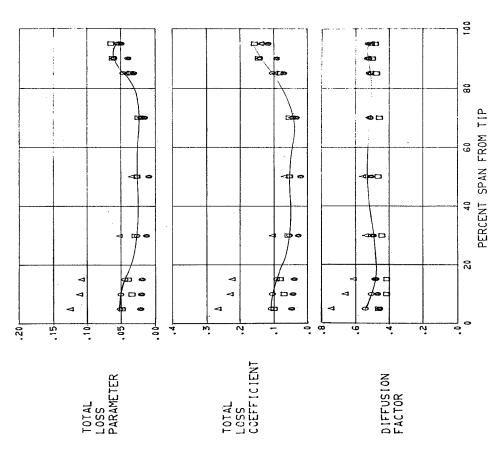


FIGURE 7. - RADIAL DISTRIBUTION OF PERFORMANCE FOR ROTOR 55B, 100 PERCENT OF DESIGN SPEED,

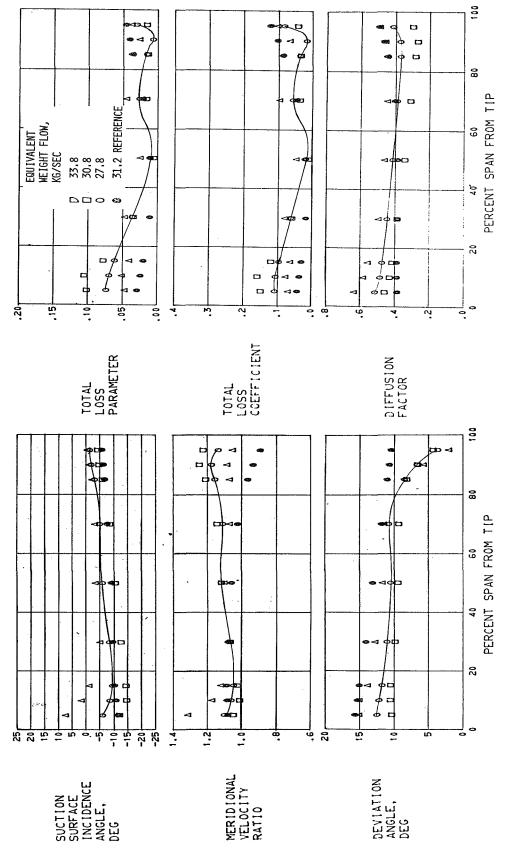
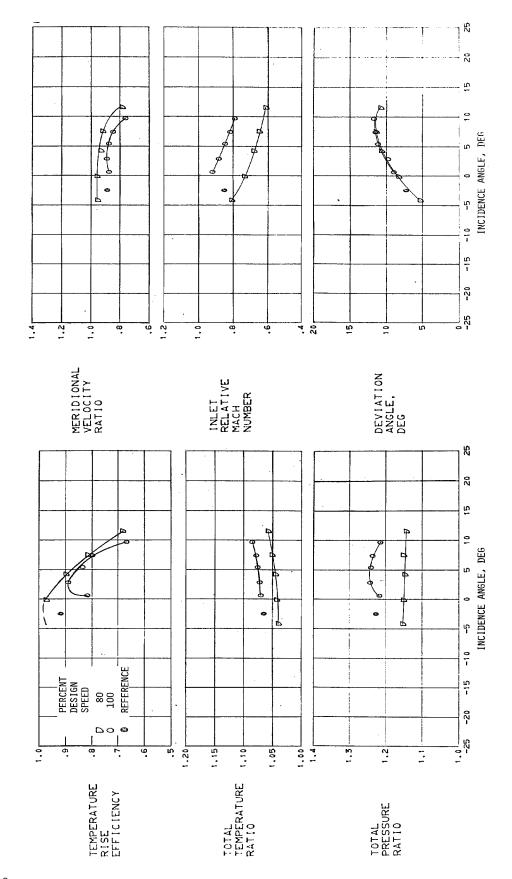
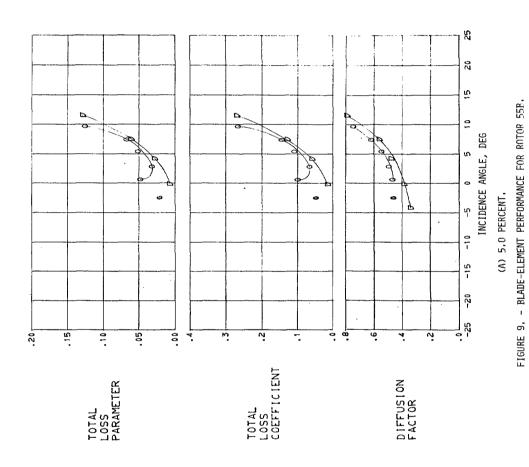
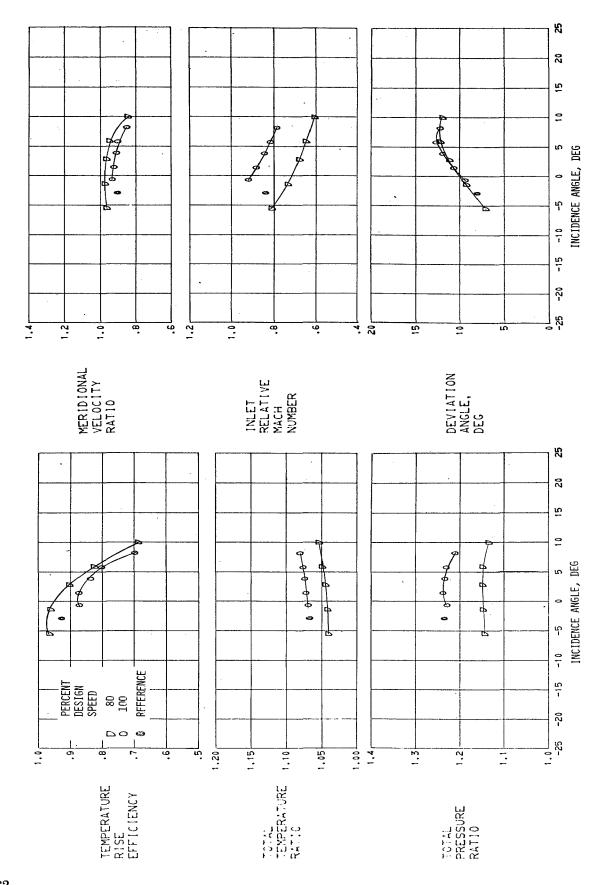


FIGURE 8. - RADIAL DISTRIBUTION OF PERFORMANCE FOR STATOR 55. 100 PERCENT OF DESIGN SPFFD.







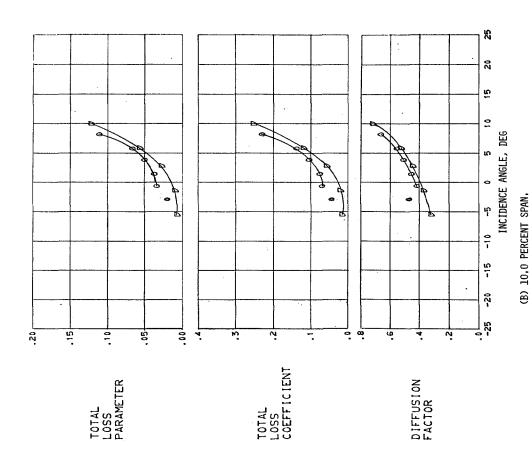
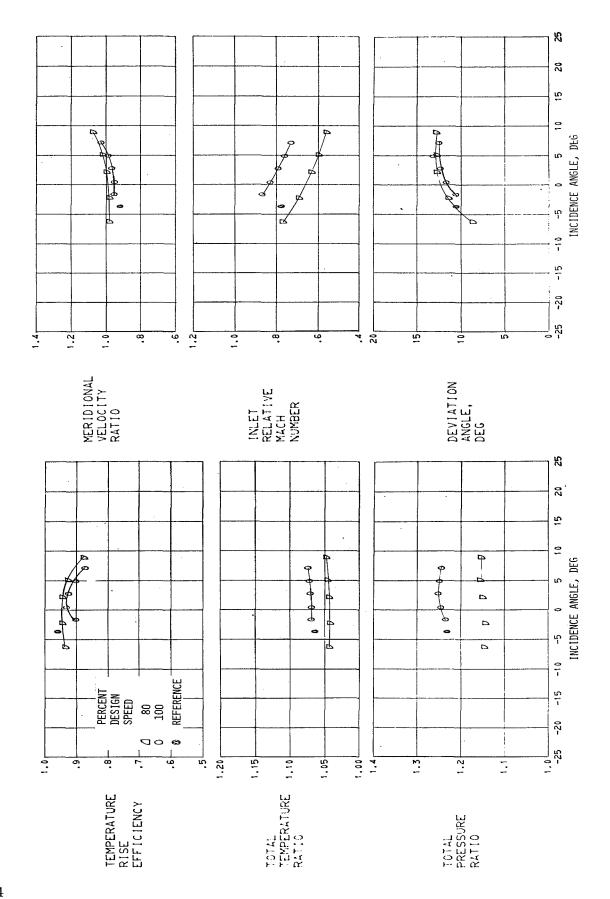


FIGURE 9. - CONTINUED. BLADE-ELEMENT PERFORMANCE FOR ROTOR 55B.



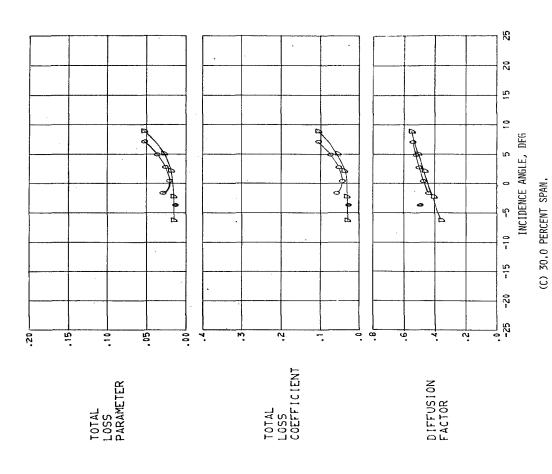
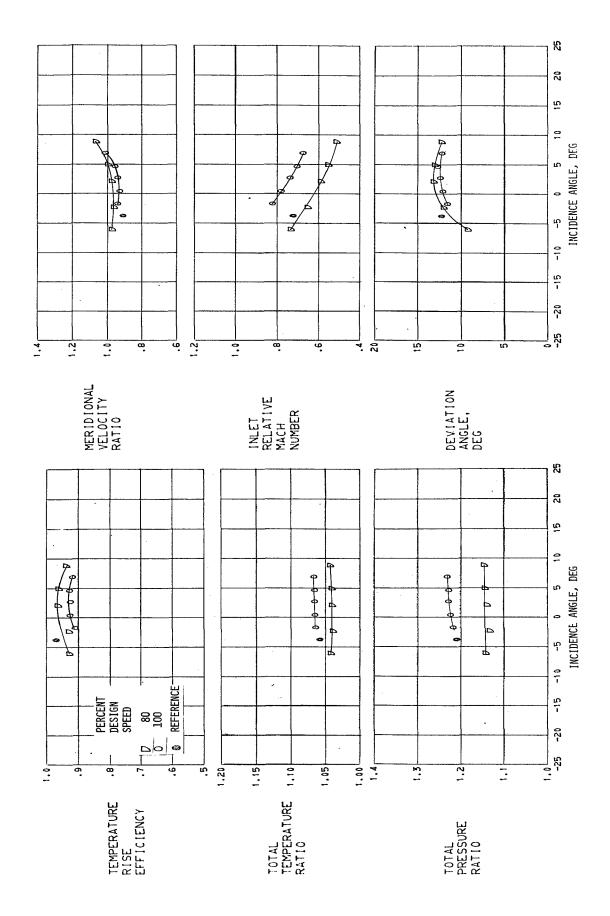


FIGURE 9, - CONTINUED, BLADE-ELEMENT PERFORMANCE FOR ROTOR 55R,



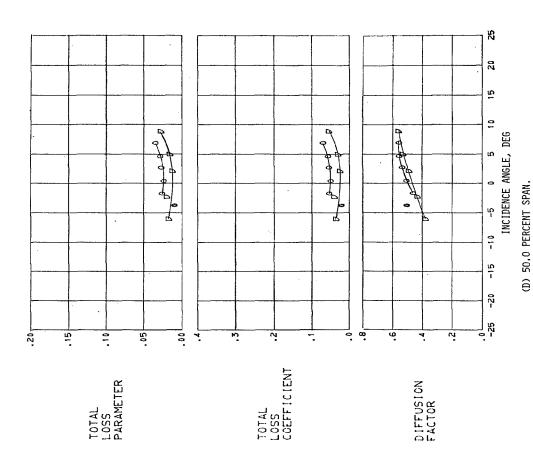
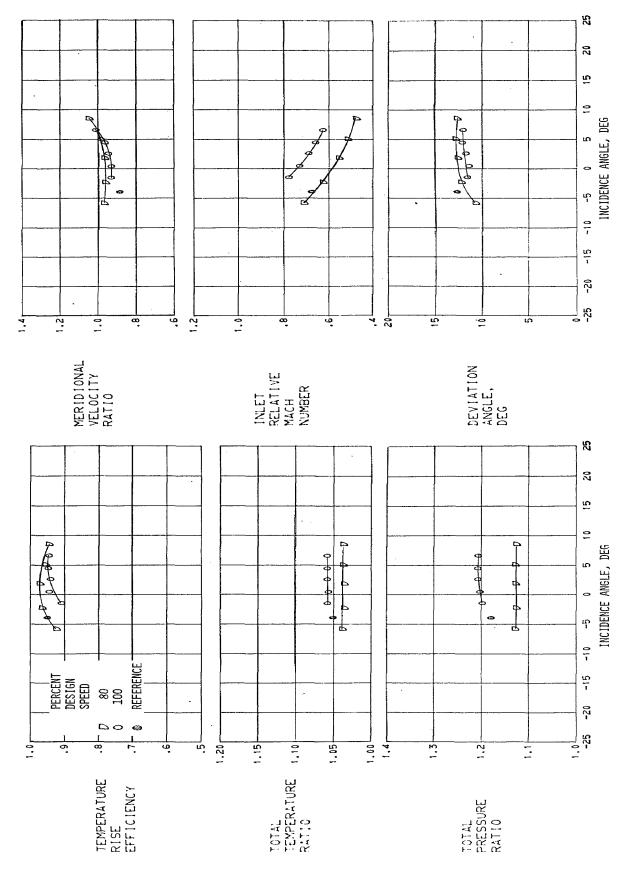


FIGURE 9. - CONTINUED. BLADE-ELEMENT PERFORMANCE FOR ROTOR 55B.



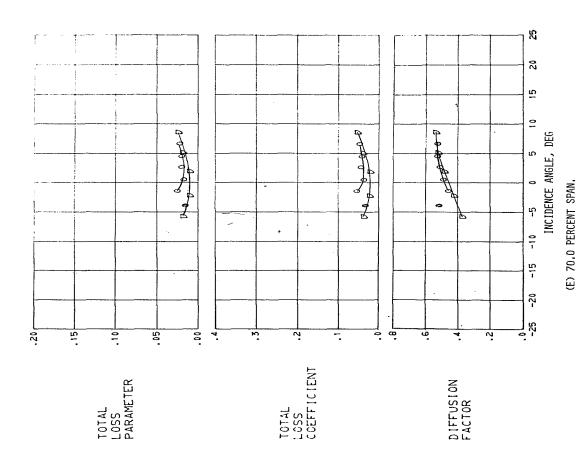
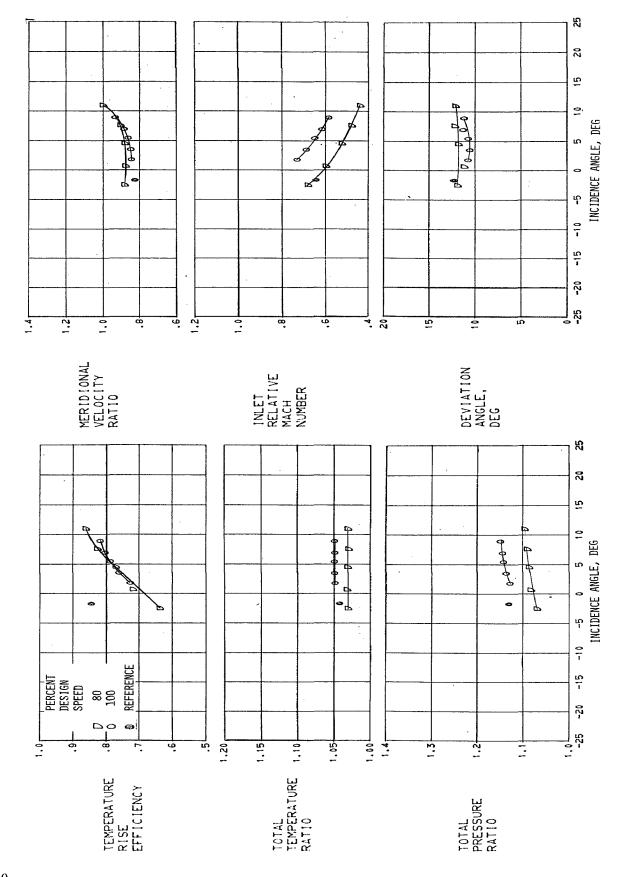


FIGURE 9, - CONTINUED, BLADE-ELEMENT PERFORMANCE FOR ROTOR 55B,



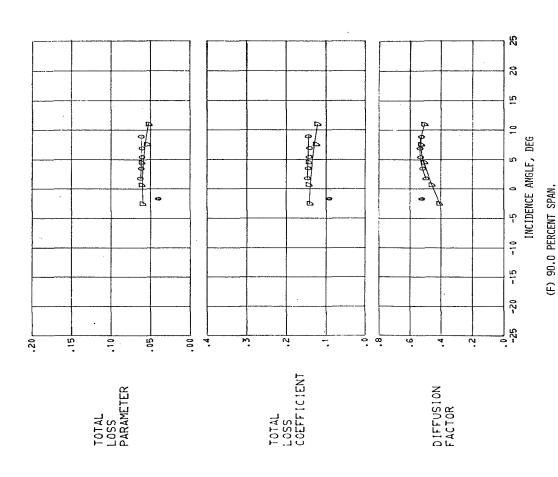
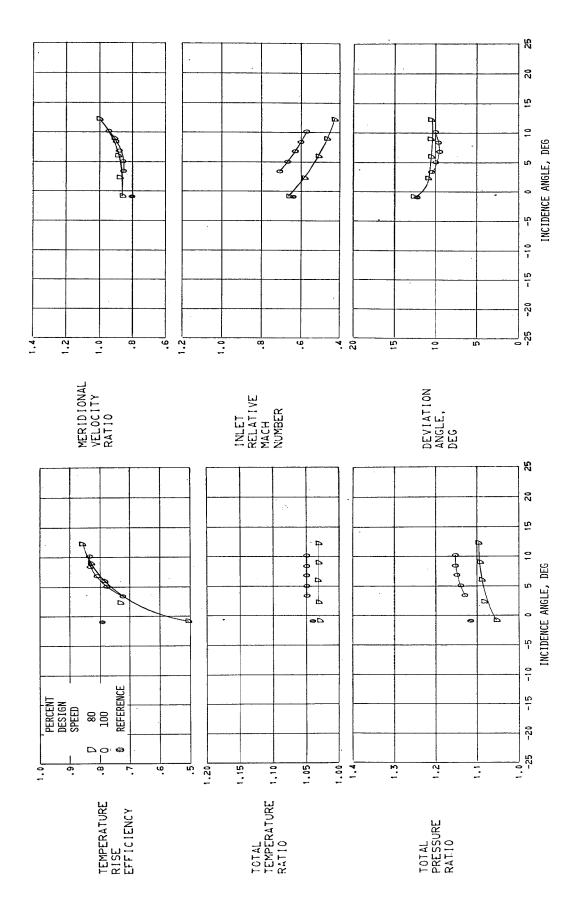


FIGURE 9. - CONTINUED. BLADE-ELEMENT PERFORMANCE FOR ROTOR 55B.



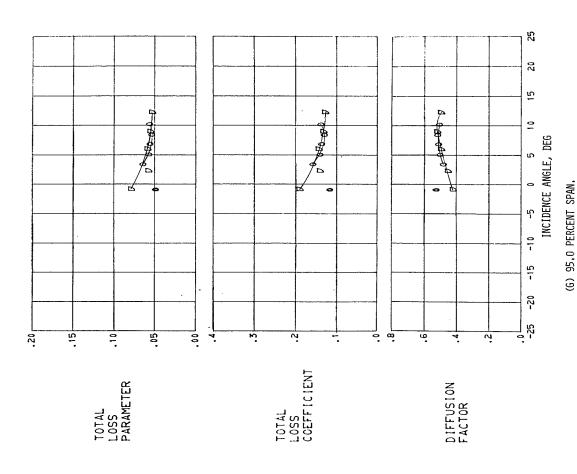
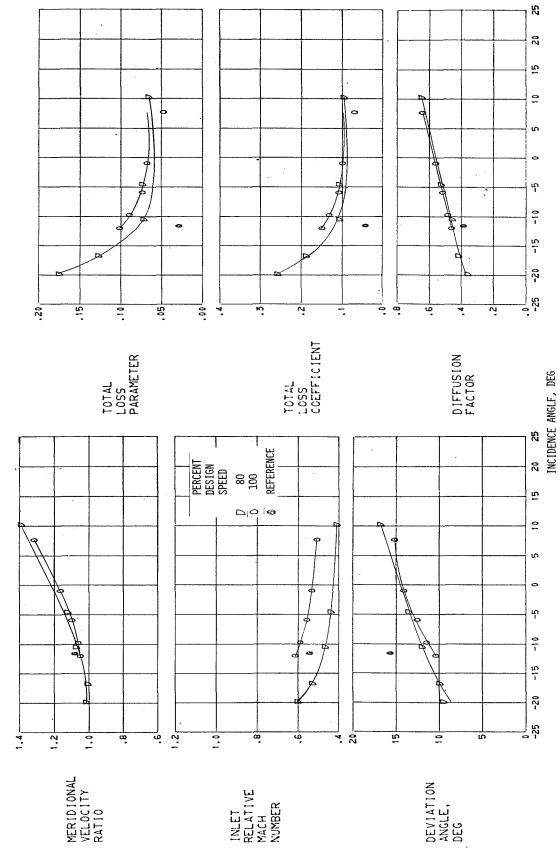


FIGURE 9. - CONCLUDED. BLADE-ELEMENT PERFORMANCE FOR ROTOR 55B,



(A) 5.0 PERCENT SPAN. FIGURE 10. - RLADE-ELEMENT PERFORMANCE FOR STATOR 55.

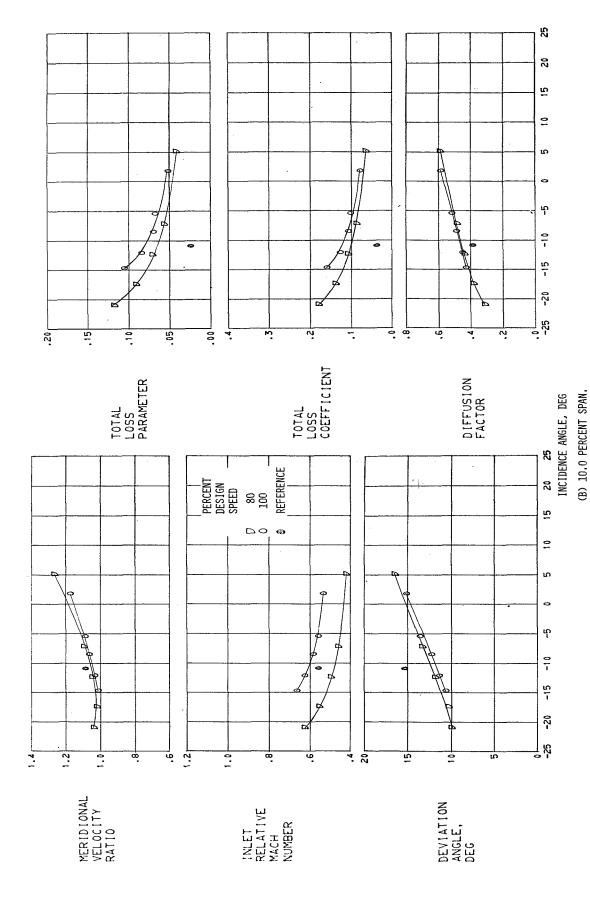


FIGURE 10. - CONTINUED. BLADE-ELEMENT PERFORMANCE FOR STATOR 55.

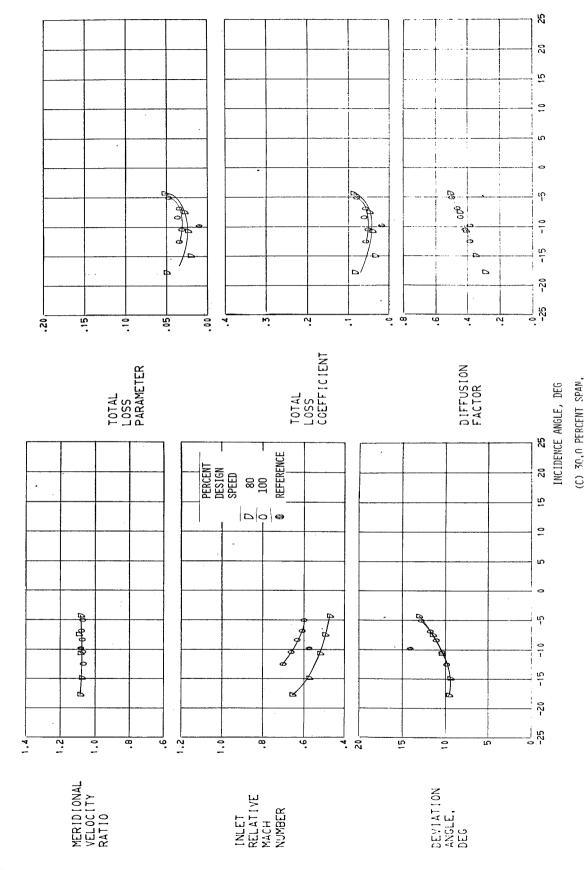


FIGURE 10, - CONTINUED, BLADE-ELEMENT PERFORMANCE FOR STATOR 55,

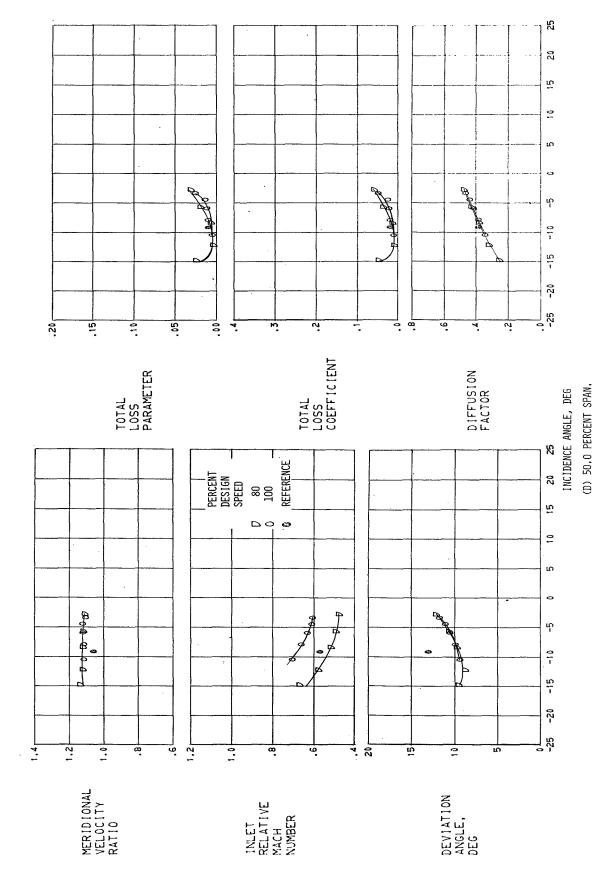


FIGURE 10. - CONTINUED. BLADE-ELEMENT PERFORMANCE FOR STATOR 55.

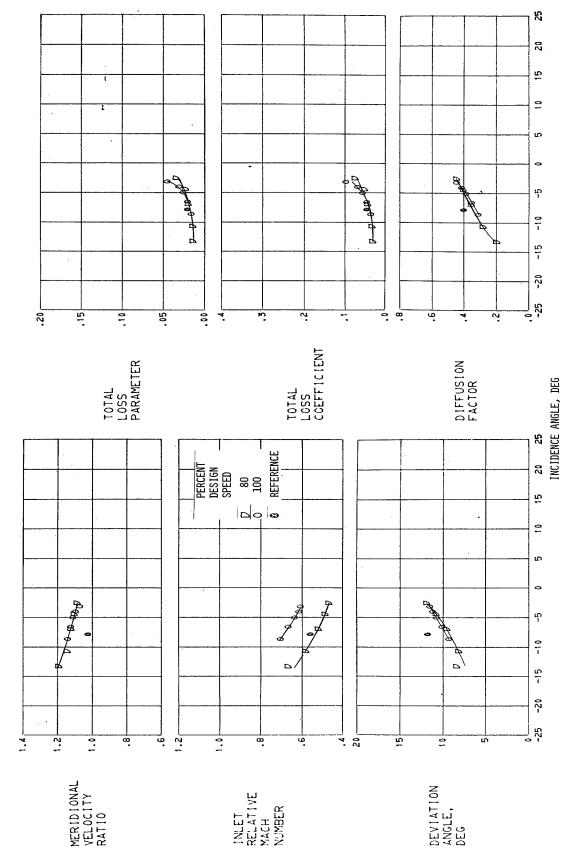


FIGURE 10, - CONTINUED. BLADE-ELEMENT PERFORMANCE FOR STATOR 55,

(E) 70,0 PERCENT SPAN.

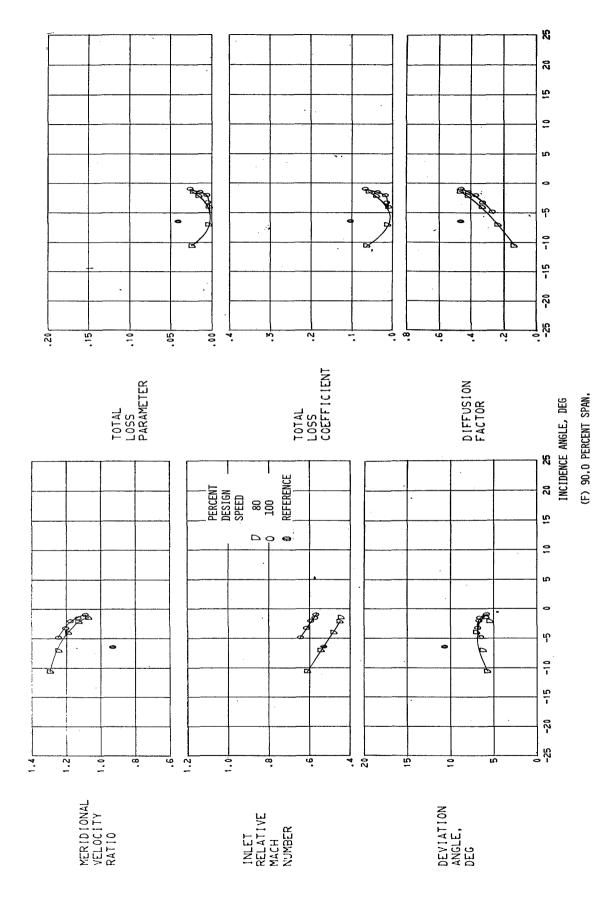
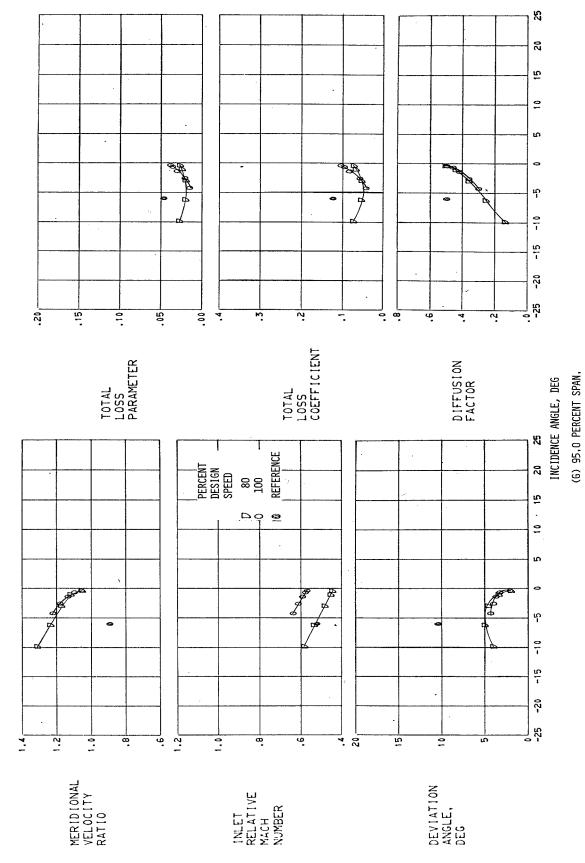


FIGURE 10. - CONTINUED. BLADE-ELEMENT PERFORMANCE FOR STATOR 55.



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FIGURE 10, - CONCLUDED, BLADE-ELEMENT PERFORMANCE FOR STATOR 55,

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